

# Bi-directional Power Converter

解鎖6.6kW SiC 雙向充電器設計

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# 6.6kW Bidirectional Power Converter Introduction



## Power & Energy Lab



**Bidirectional Charger (250-450V/19.6A, 6600W) for EV, PFC**

P/N : 2021P004-ST



Released

Functions	Qty	Charger for EV
SIC MOS	16	SCTW40N120G2VAG- SCT040W120G3-4AG
SIC MOS Gate Driver- 1-CH	12	STGAP2SICS
Gate Driver Isolated Power	12	A6986I*
Aux -30W	1	VIPER31*
Isolated DC-DC/10W	6	STL8N10LF3*
MCU	1	STM32G474VBT6

## Automation Lab

**IO-link Master**



**8-CH Master w/ Arrow MCU**

P/N : 2021W001



Released

8-CH IO-link Master	Qty
ARW-IOLM4P-STM32L4 STM32L431RBT6	2
M24256-BRDW6TP	2
USBLC6-4SC6	1
L7986ATR	1
LD1117S33TR	1
LD39050PU33R	1
M93C66-RMC6TG	1
IPS161H	8
L6360	8
SPT01-335DEE	8
STM32F746ZGT6	1
STG3693QTR	2

**IO-link Slave – Sensors/ Actuators**

**8-CH Digital Input**

P/N : 2021W002



Released

DI Module	Qty
SM15T33CA	1
SMA4F5_0A	1
STM32G071RBT6	1
STISO621WTR	2
CLT01-38SQ7-TR	1
L7986ATR	1
SPT01-335DEE	1
LD39050PU33R	1
L6364Q	1
STPS140Z	8
STPS3L60UFN	1
STPS340AFN	1

**8-CH Digital Output**

P/N : 2021W003



Released

DO Module	Qty
STPS3L60UFN	1
STPS340AFN	1
SM15T33CA	1
SMA4F5_0A	1
L7986ATR	1
SPT01-335DEE	1
LD39050PU33R	1
L6364Q	1
ISO8200AQ	1
STM32G071RBT6	1

**Tower-light CTRL**

P/N : 2021W005



Released

Tower light	Qty
IPS4260L	1
L6364Q	1
STM32G071	1
M24C08	1
SMB15F24A	2
STG3157CTR	1

**8CH Master w/ Profinet Software version** In Development

## Motor Control Lab



**Air-conditioning Compressor**

P/N : 2019M002 Customization



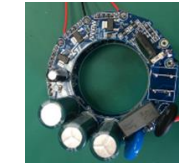
STEVAL-CTM010V1

Released

Func.	HVAC – 2kW	Qty
IPM	STGIB15CH60TS-L	1
MCU	STM32F302RBT6	1
PFC MOS	STP4LN80K5	2
PFC Gate DRV	PM8834	1
PFC Diode	STTH30AC06C	2
TRIAC	T435-800B	1
Valve Stepper Motor CTRL	STSPIN820	1

**110 krpm BLDC Motor Driver**

P/N : 2021M001



Released

Func.	Fast Hair Dryer	Qty
MCU +GATE DRV	STSPIN32F0601Q	1
MOS	STN6N60M2	6
AUX	VIPER222	1
LDO	LD1117S33TR	1
AUX Diode	BAT41ZFILM	1
AUX Pri. Diode	STTH1L06A	2
TRIAC	T1635T-8FP	1

**1kW Servo Motor Driver**

P/N : 2022M001



Newly released Q3'22

Func.	Servo	Qty
MCU+GATE DRV	STSPIN32G4	1
MOS	STL110N10F7	6
AUX	VIPER319HDTR	1
AUX Diode	STPS1H100A	3
DC-DC	ST1540IDR	2
LDO	LD1117S12TR	1
Ethernet Protection	ETP01-1621RL	4
Quad. RS-42X	ETP01-1621RL	2



**Energy Storage (ESS) bi-directional 80V/82.5A Output, 6600W, PFC & DC-DC**

P/N : 2021P005-ST, 2021P006-ST



Off-grid PFC Newly released Q3'22



DC-DC Q4'22 release In Development

Functions	Qty	Energy Storage
SIC MOS	16	SCTWA60N120G2-4 -> SCT040W120G3-4AG
SIC MOS Gate Driver- 1-CH	8	STGAP2SICS
Gate Driver Isolated Power	12	A6986I
DC-DC low side FET	32	STP75NF20
Aux	1	VIPER319HDTR
Diode	2	STPS1150A
Digital Isolator	2	STISO621WTR
Isolated DC-DC/10W	6	STL8N10LF3*
ESD Suppression	3	HDMIULC6-4SC6Y
ESD Suppression	2	ESDCAN03-2BWY
MCU	2	STM32G474VBT6

**11 kW Battery Formation bidirectional-48V**

P/N : 2022P001



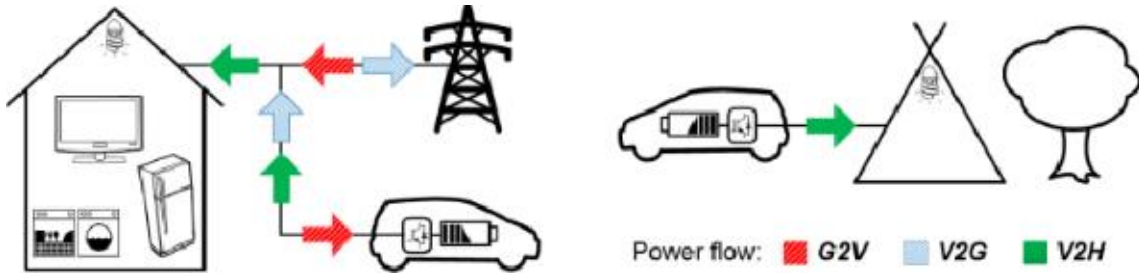
In Development

Functions	15kW PFC	Qty
HV SiC MOS	SCT040W120G3-4AG	6
SiC MOS	SCT018W65G3-4AG	6
MCU	STM32G474VBT6	1
Gate DRV	STGAP2SM	12
AUX	VIPER26HD	1

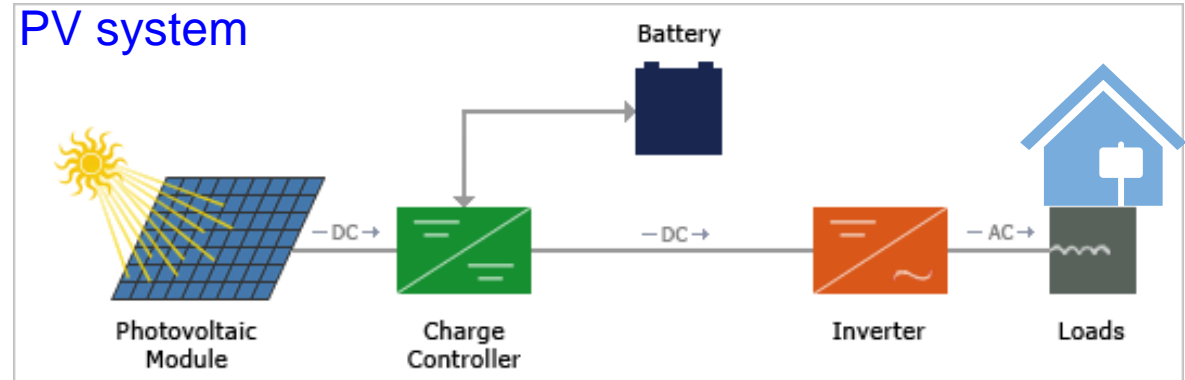
# 6.6kW Bidirectional Power Converter Introduction

## Application examples:

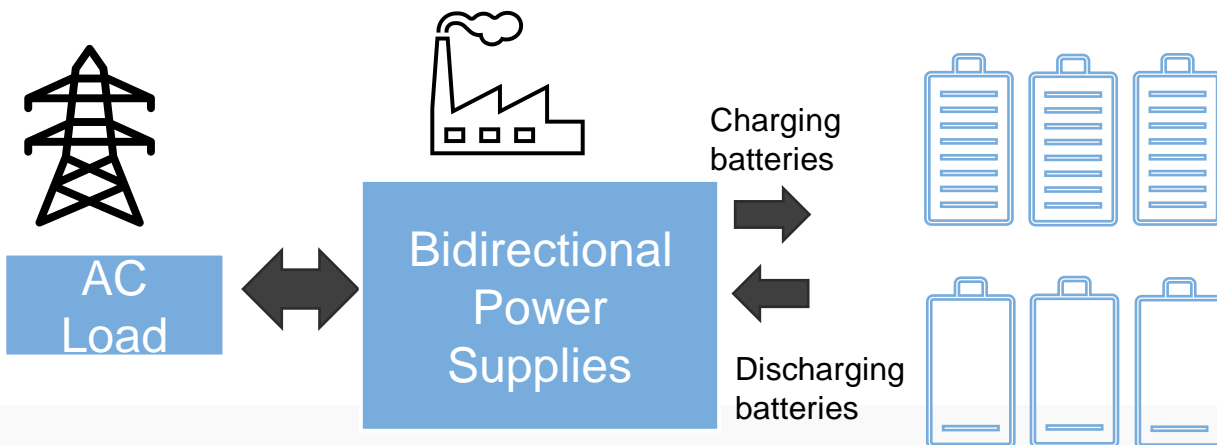
### EV system



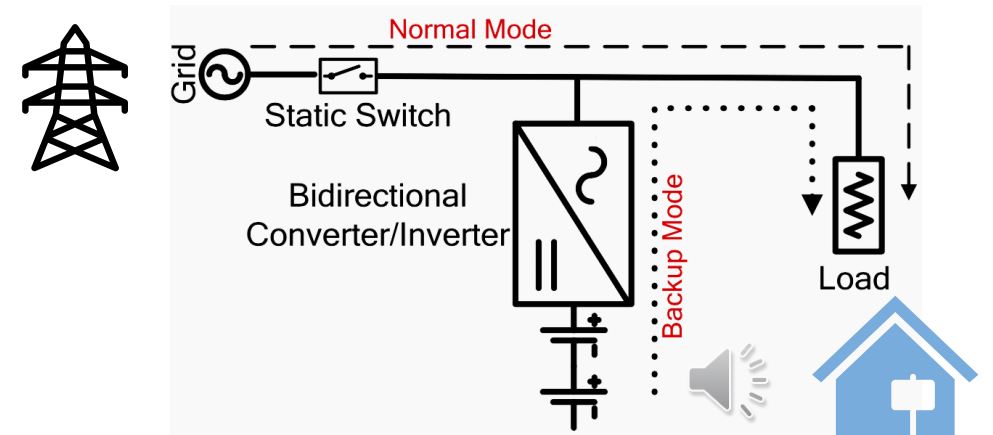
### PV system



### Equipment- e.g. Battery formation, Aging Test Loading



### Energy storage system/ Emergency Power Supplies



# Block Diagram - Bidirectional charger for EV- 250-450V, 19.6A/ 6600W



AC-DC board

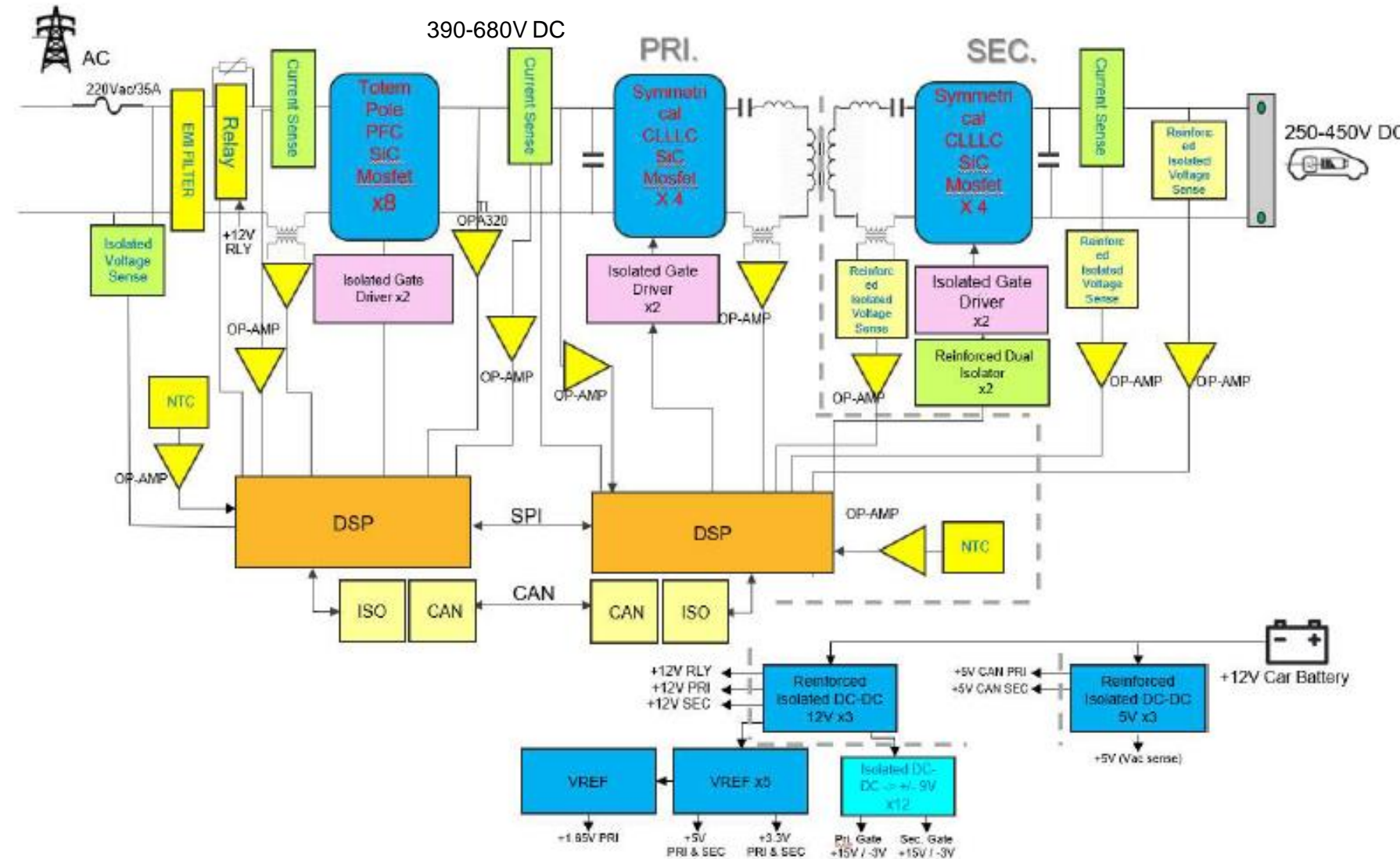
DC-DC board

## Specification:

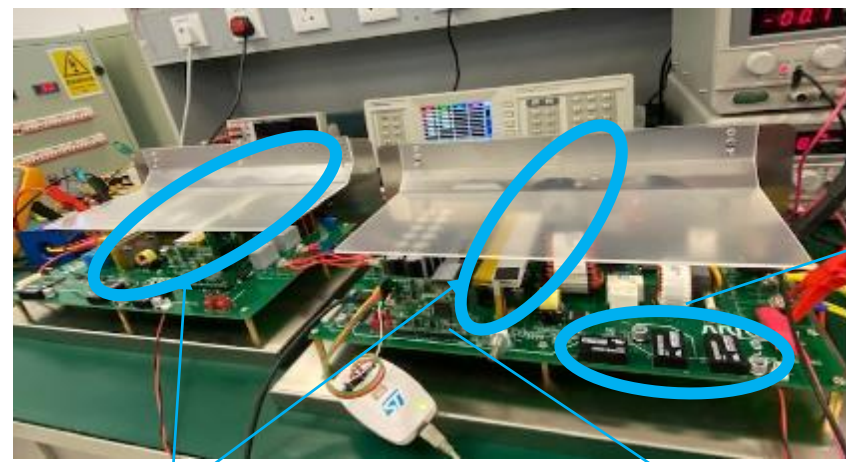
- AC/DC Bidirectional Power Conversion
- Max Charging Power: 6.6kW
- AC Input Voltage: 200-265 VAC
- DC Output Power: 250-450VDC
- Max Inversion Power: 3.3kW
- Inversion Rated Input: 336Vdc
- Inversion rated Output: 220Vac 50Hz
- Efficiency >95%
- Totem Pole PFC 67kHz
- CLLLC 200kHz

## Applications:

- Onboard charger for EV
- Bidirectional AC-DC equipment
- Energy Storage

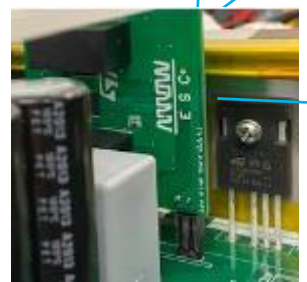
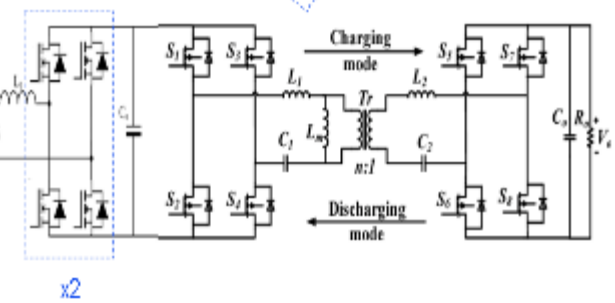
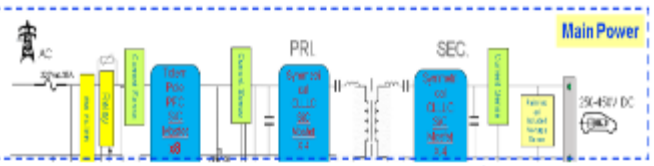


# 1) Power Conversion – Bidirectional charger - 250-450V, 19.6A/ 6600W



**Isolated power supply with STL8N10LF3 (2021)**  
**Specification:**

- $V_{in} = 12Vdc$
- $V_{out} = 12V, 1.1A (Max)$



ST SiC MOS & Gate Driver Board



SiC MOS Gate Driver



ST MCU Board

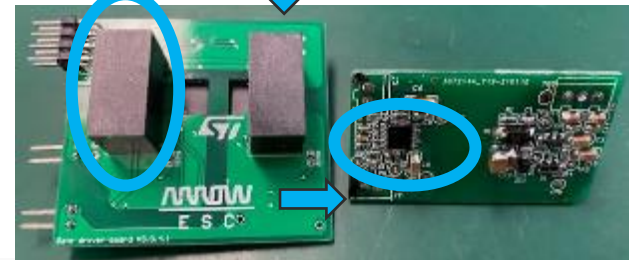
■ Key ST Parts

Functions at p	Qty	Devices
SiC MOS	16	SCTW40N120G2VAG
SiC MOS Gate Driver-1-CH	12	STGAP2SiCS
Gate Driver Isolated Power	12	A69861*
Aux -30W	1	VIPER31*
Isolated DC-DC/10W	6	STL8N10LF3*
MCU at PFC Bd.	1	STM32G474VBT6

ARROW Demo Video



YouTube Youku 优酷



Gate Driver Isolated Power Module  
 Discrete Alternatives by ST-A69861



ST Aux Power -30W-ST-VIPER31

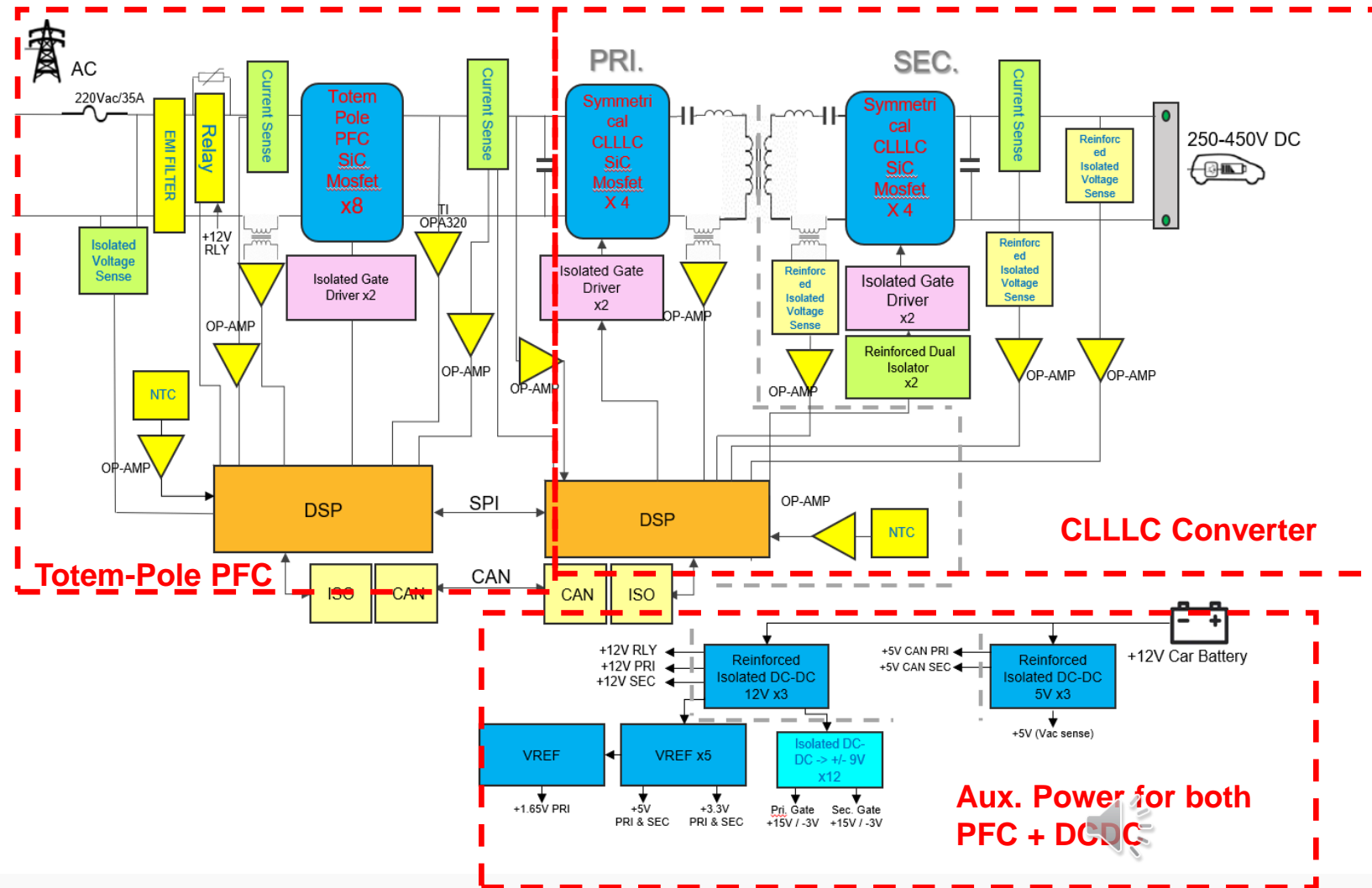


Arrow proprietary information – Selective Disclosure only

# 6.6kW Bidirectional Power Converter Block Diagram

## Challenges

1. Noise at SiC MOSFET gate driving
2. PFC current spike issue at zero-crossing
3. Vac drop (Under-voltage control)
4. CLLLC secondary synchronous rectifier control



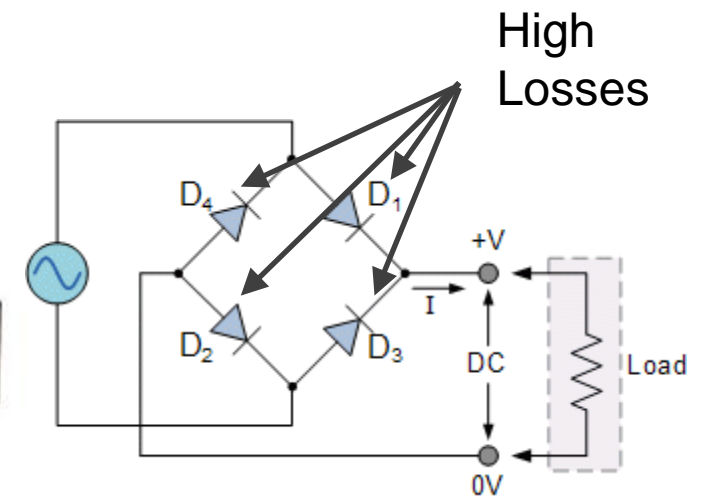
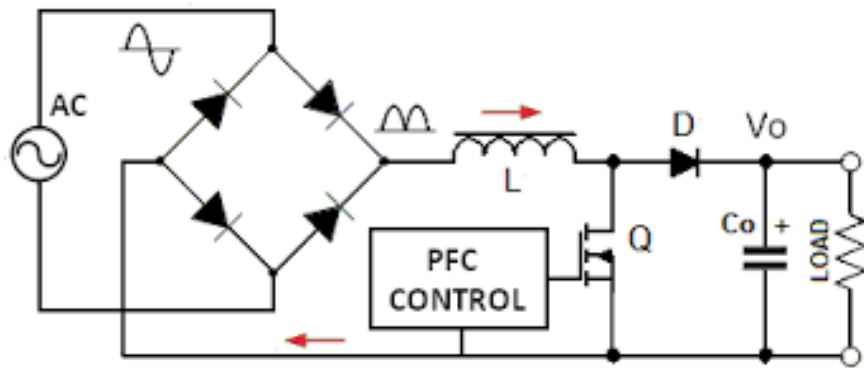


# Totem-Pole PFC Bidirectional Power Converter

# Why Totem Pole PFC?

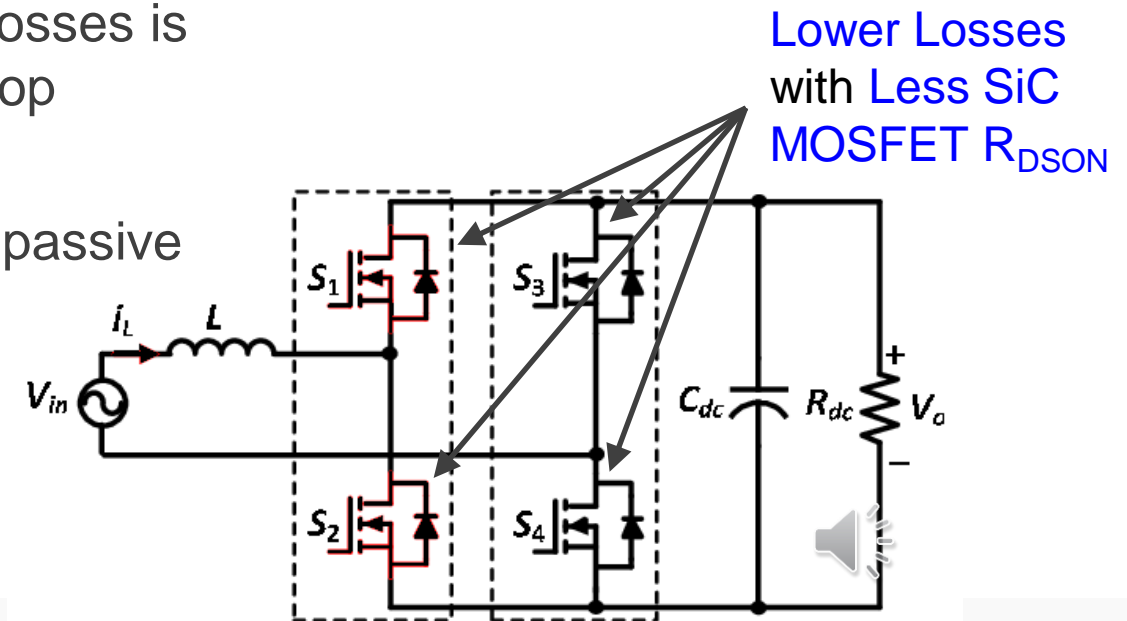
## Disadvantages of Traditional PFC :

- Larger sized passive components are used
- Higher conduction losses at bridge rectifiers and passive components



# Totem-Pole PFC Bidirectional Power Converter

- Totem-Pole PFC is always called Bridgeless Totem-Pole PFC or Bridgeless PFC
- Advantage:
  - ✓ Capability of bidirectional power transfer
  - ✓ MOSFET substituted the bridge rectifier,  $R_{DSON}$  losses is lower than the bridge rectifier forward voltage drop
  - ✓ SiC MOSFET used, lower power loss
  - ✓ Higher frequency, smaller ripple, smaller size of passive components can be used
  - ✓ Higher power density



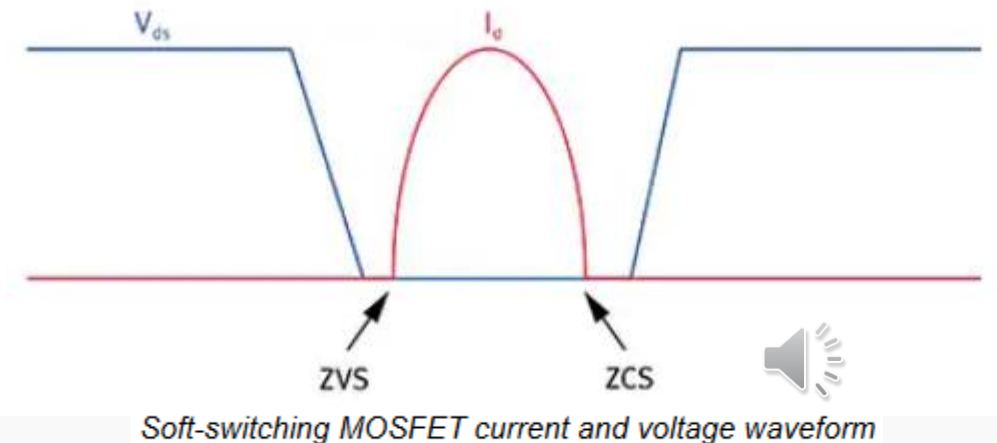
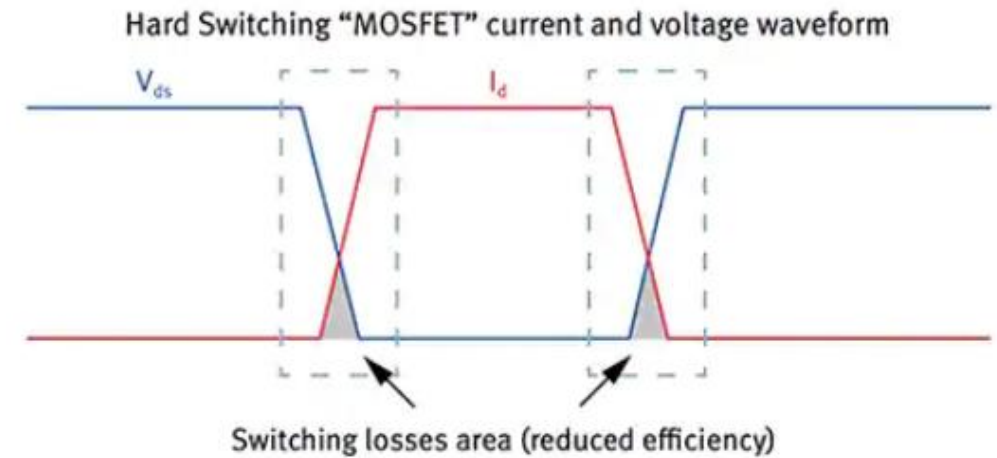
# CLLLC Full Bridge Bidirectional Power Converter



# CLLLC Full Bridge Bidirectional Power Converter

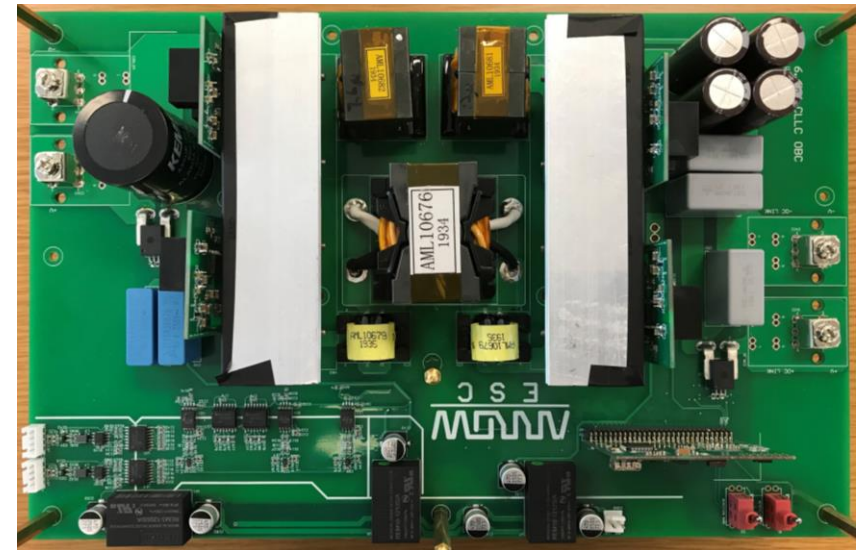
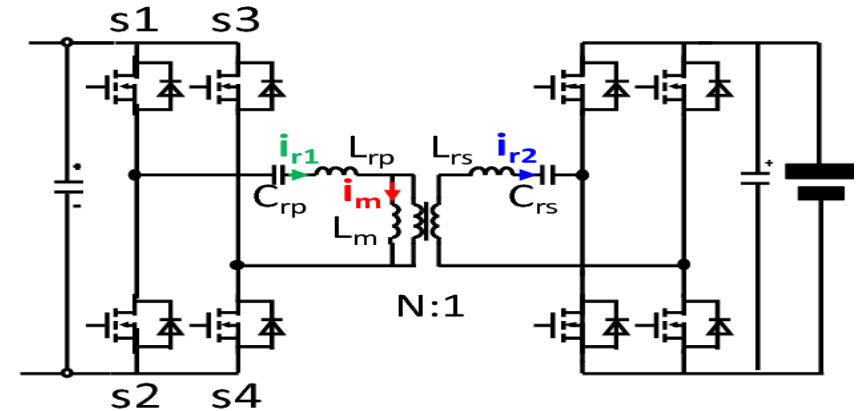
## Why CLLC?

- Soft-switching by Zero Voltage Switching (ZVS) and Zero Current Switching (ZCS)
- Without ZVS and ZCS, the large switching losses when current and voltage are overlapped at switching
- With ZVS and ZCS, no current and voltage overlapping at switching



# CLLLC Full Bridge Bidirectional Power Converter

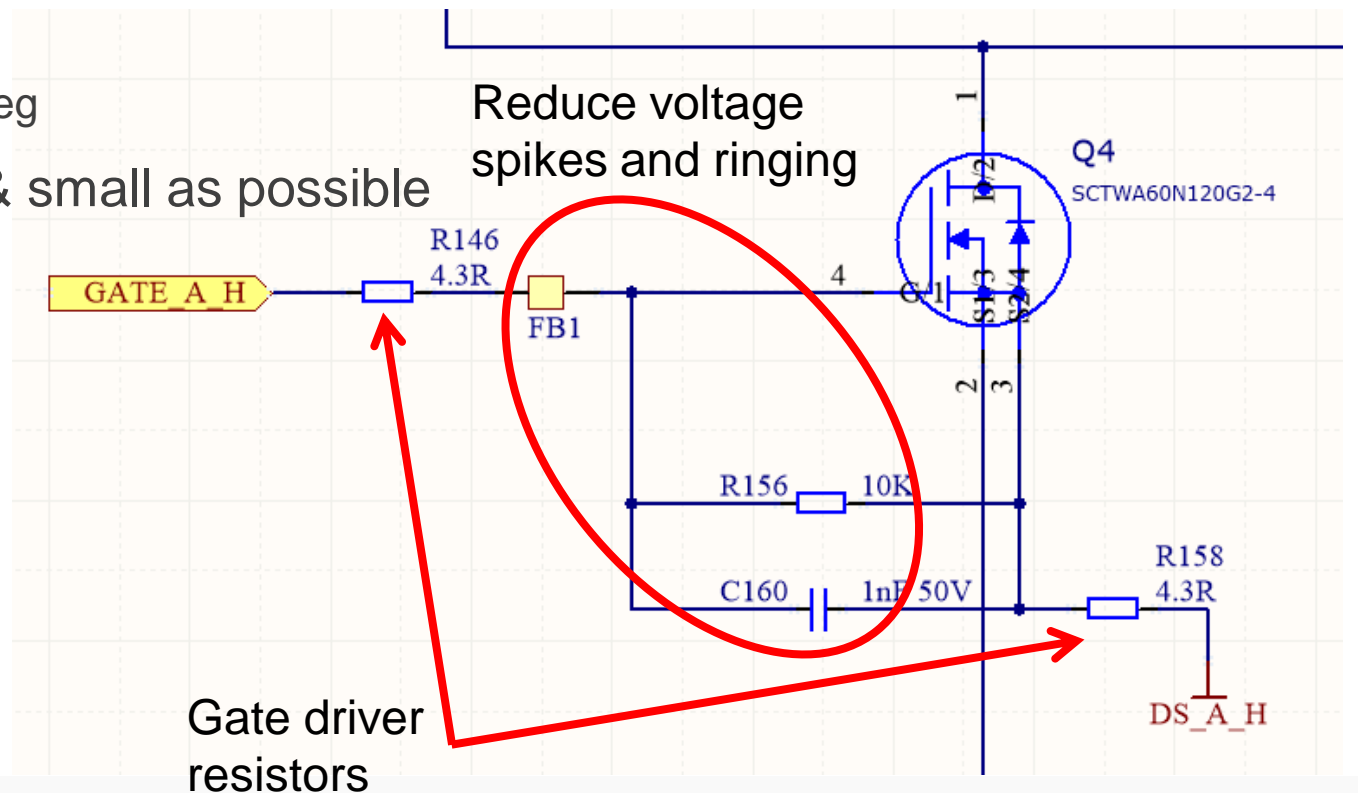
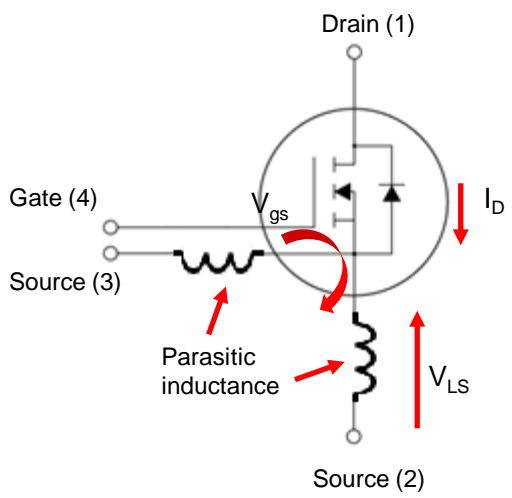
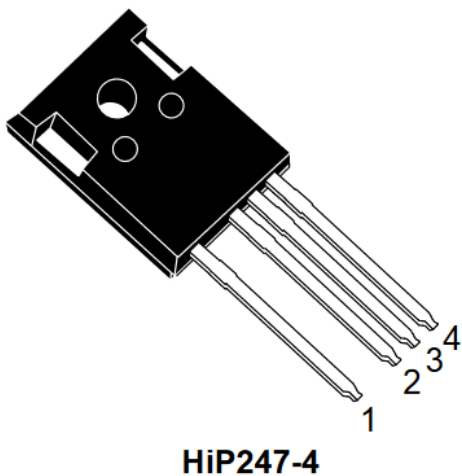
- CLLLC is a Resonant, Soft-switching Power converter topology
- Advantages:
  - ✓ Capability of bidirectional power transfer
  - ✓ ZVS / ZCS soft switching technologies to achieve lower power loss
  - ✓ Higher switching frequency, smaller ripple
  - ✓ SiC MOSFET used, lower  $R_{dson}$ , lower power loss
  - ✓ Smaller size passive components can be used
  - ✓ Higher power density
  - ✓ Symmetrical, easier to control
- CLLLC vs LLC
  - LLC has less components, but more complex in control for Gain/Q-point control, especially in reverse direction (inverter mode)
    - LLC in reverse direction (inverter mode) at primary, not ZVS, it's hard-switching, as there is no resonant tank



# SiC MOSFET & Gate Driver Design

# Design challenge: Noise at SiC MOS Gate Driving

- SiC MOSFET: SCTWA60N120G2-4 (1200V; 35mΩ typ.; 60A; **HiP247-4**; )
  - Two separate Source to separate Gate-Source (G-S) Control Loop and (Drain-Source) Power Loop
- Optimized Gate driver circuit for SiC MOSFET to prevent gate oscillation and reduce voltage spikes and ringing
  - Ferrite Bead at Gate, but not at the Gate Leg
- PCB wiring- G-S & D-S loop as short & small as possible





# SiC MOSFET & Gate Driver

- SiC MOSFET needs positive & negative voltage driving supply e.g. +20V / -5V

- Discrete design- ST A6986I

- Simple circuit; Size optimized; Fully isolated
- No special feedback circuit is needed
- +12Vdc input voltage; +20Vdc / -5Vdc output voltage
- Max. output power 2.5W
- Discrete solution is more cost effective

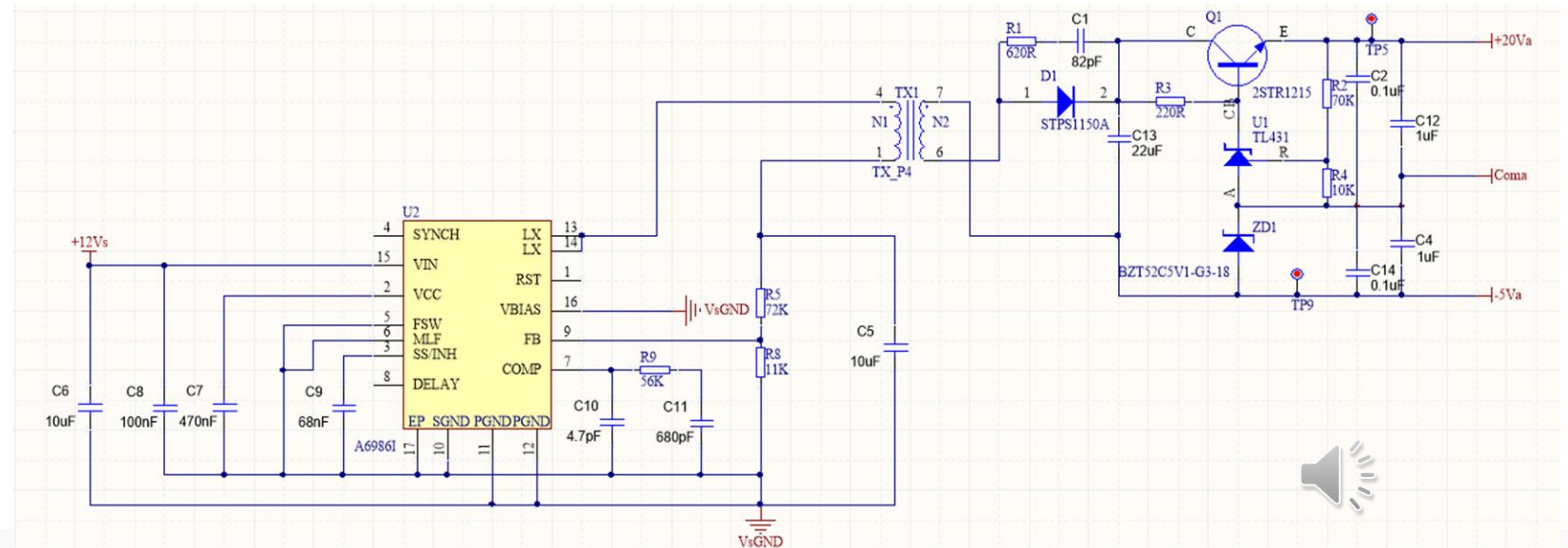


ST SiC MOS & Gate Driver Board

SiC MOS Gate Driver



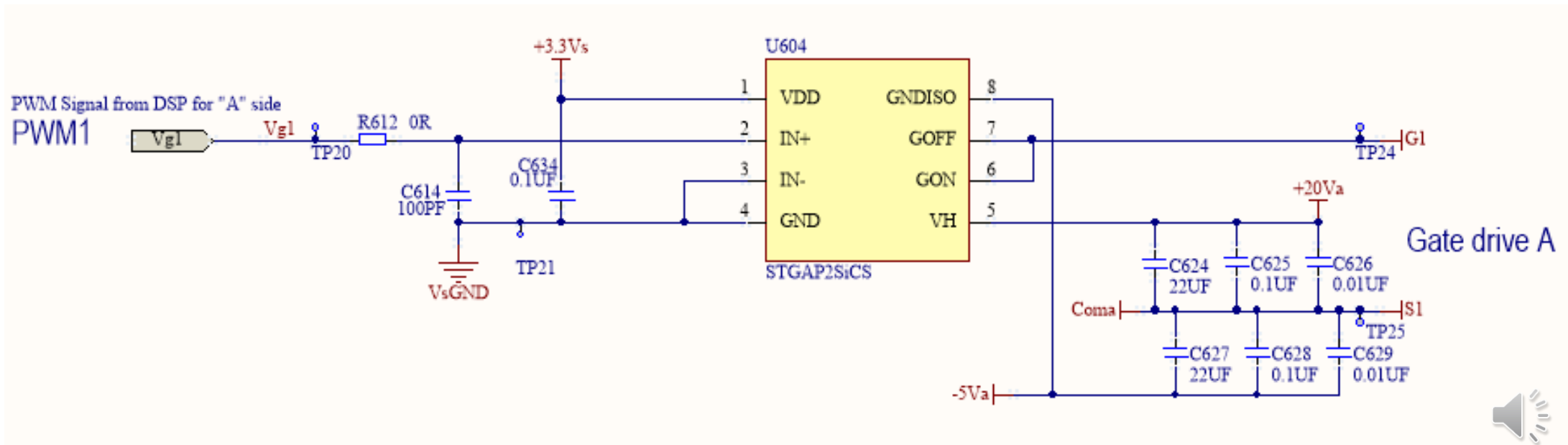
Gate Driver Isolated Power Module  
Discrete Alternatives by ST-A6986I



# SiC MOSFET & Gate Driver

## Gate driver – ST STGAP2SiCS

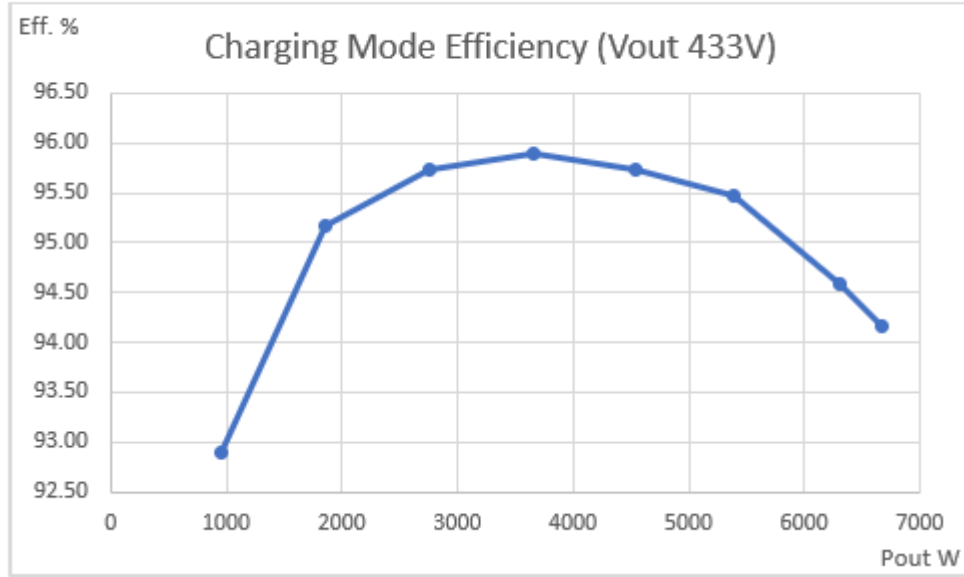
- 4 A driving capability
- Miller CLAMP function prevents gate driver spikes during fast switching operation
- Integrated protection: UVLO & Thermal shut down
- Input to output propagation delay less than 75 ns



# Test Results

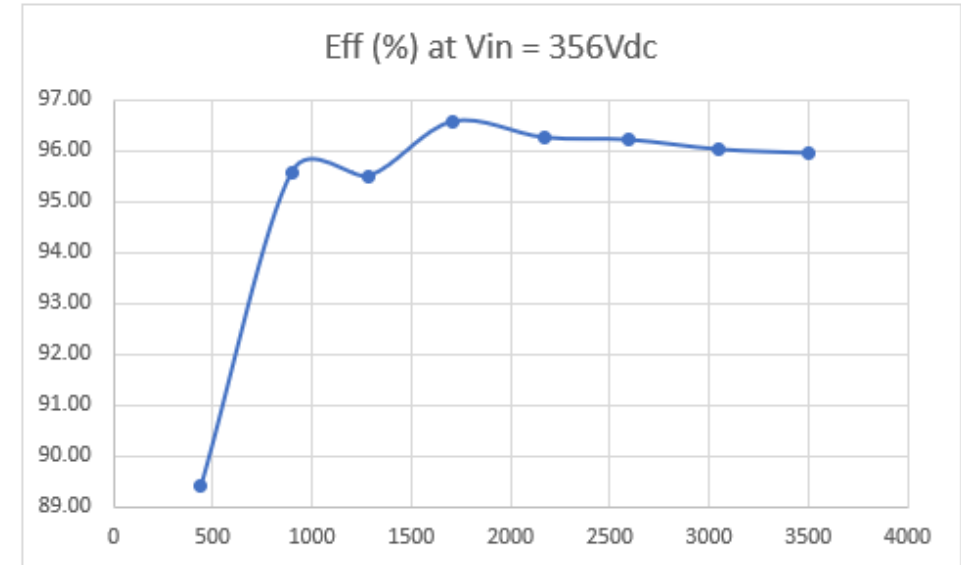
# Bidirectional Charger for EV- 250-450V, 19.6A/ 6600W Test Results

Charging Mode:



Vin (V)	230	230	229	229	229	229	228	228
Pin (W)	1028	1950	2885	3818	4741	5646	6675	7076
Vout (V)	433	432	431	430	429	427	426	425
Pout (W)	955	1856	2762	3661	4539	5390	6314	6663
PF	0.986	0.995	0.996	0.997	0.998	0.998	0.998	0.998
Eff (%)	92.9	95.18	95.74	95.89	95.74	95.47	94.59	94.16

Inversion Mode:



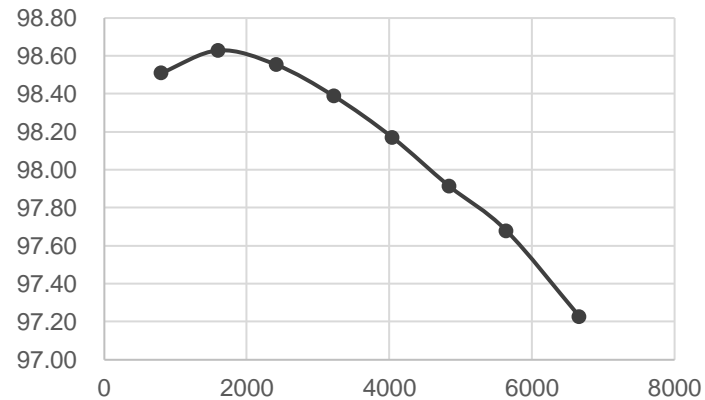
Vin (V)	355.92	355.85	355.72	355.72	355.69	355.49	355.47	355.28
Pin (W)	493.86	938.19	1347.30	1767.10	2251.30	2697.00	3175.00	3643.60
Vout (Vac)	222.85	218.30	217.85	217.00	216.81	216.95	216.61	215.97
Pout (W)	441.58	896.74	1286.90	1706.70	2167.30	2595.20	3049.00	3496.40
PF	0.9565	0.9896	0.9948	0.997	0.9981	0.9983	0.9988	0.9989
Eff (%)	89.41	95.58	95.51	96.58	96.27	96.22	96.03	95.96

# Bidirectional Charger for EV- 6600W (PFC board only)

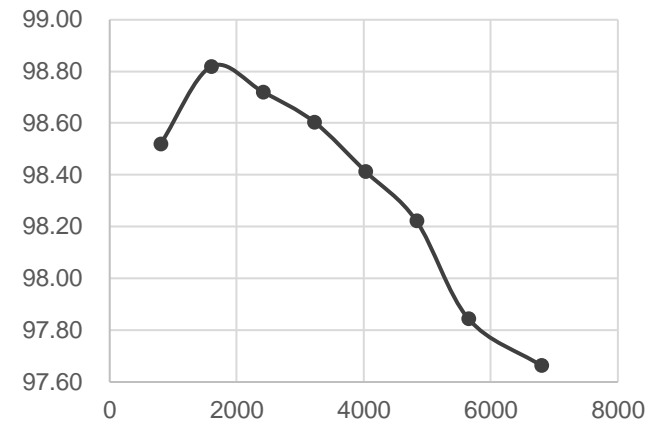
## Test Results

- Efficiency of PFC at  $V_{in}= 200/220/230/260V_{ac}$  and  $V_{out} = 400V_{dc}$

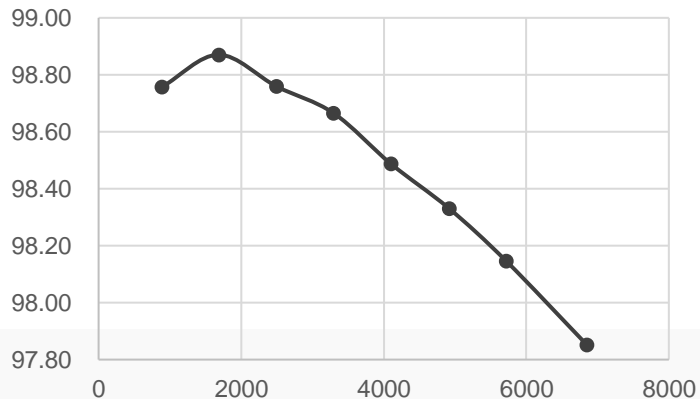
$V_{in\_200V}$  &  $V_{out\_400V}$



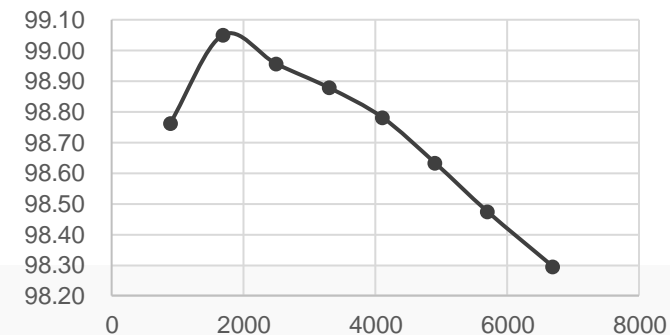
$V_{in\_220V}$  &  $V_{out\_400V}$



$V_{in\_230V}$  &  $V_{out\_400V}$



$V_{in\_260V}$  &  $V_{out\_400V}$

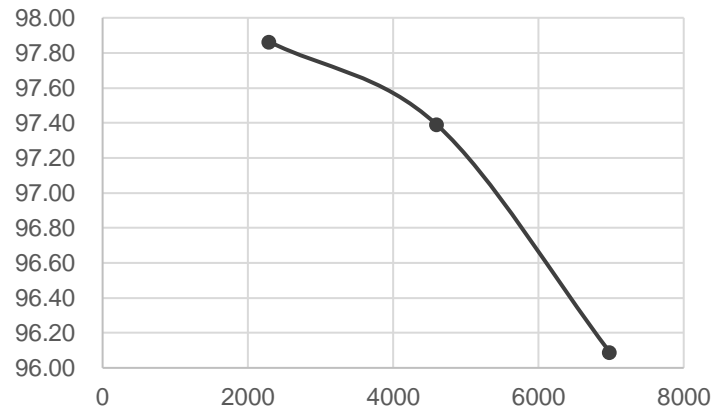


# Bidirectional Charger for EV- 6600W (PFC board only)

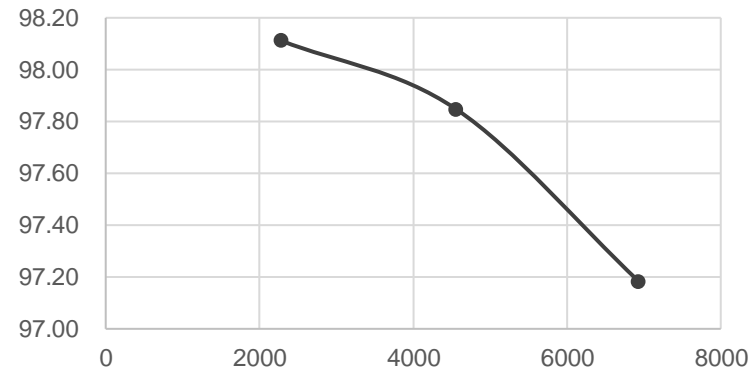
## Test Results

- Efficiency of PFC at  $V_{in}= 200/220/230/260V_{ac}$  and  $V_{out} = 680V_{dc}$

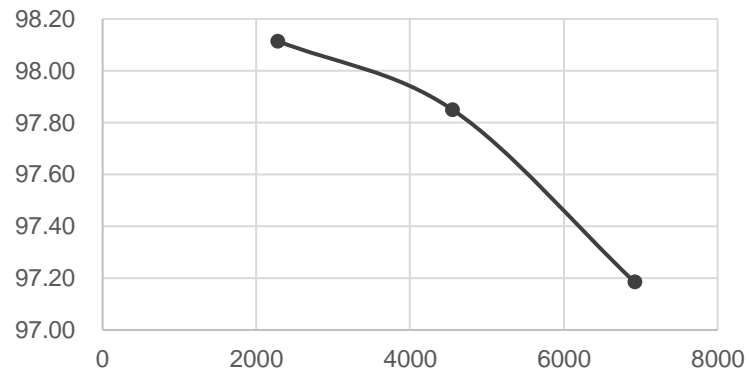
$V_{in\_200V\&V_{out\_680V}}$



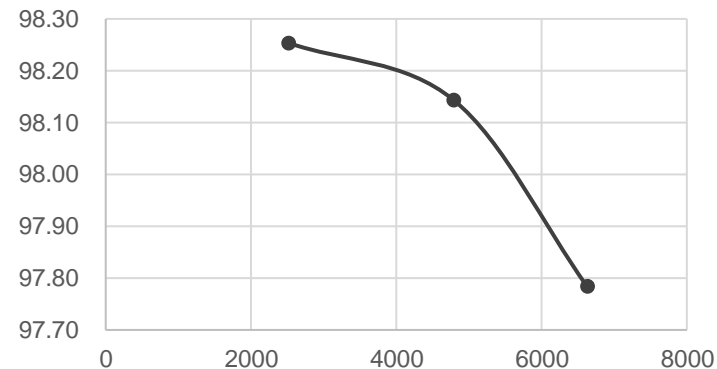
$V_{in\_220V\&V_{out\_680V}}$



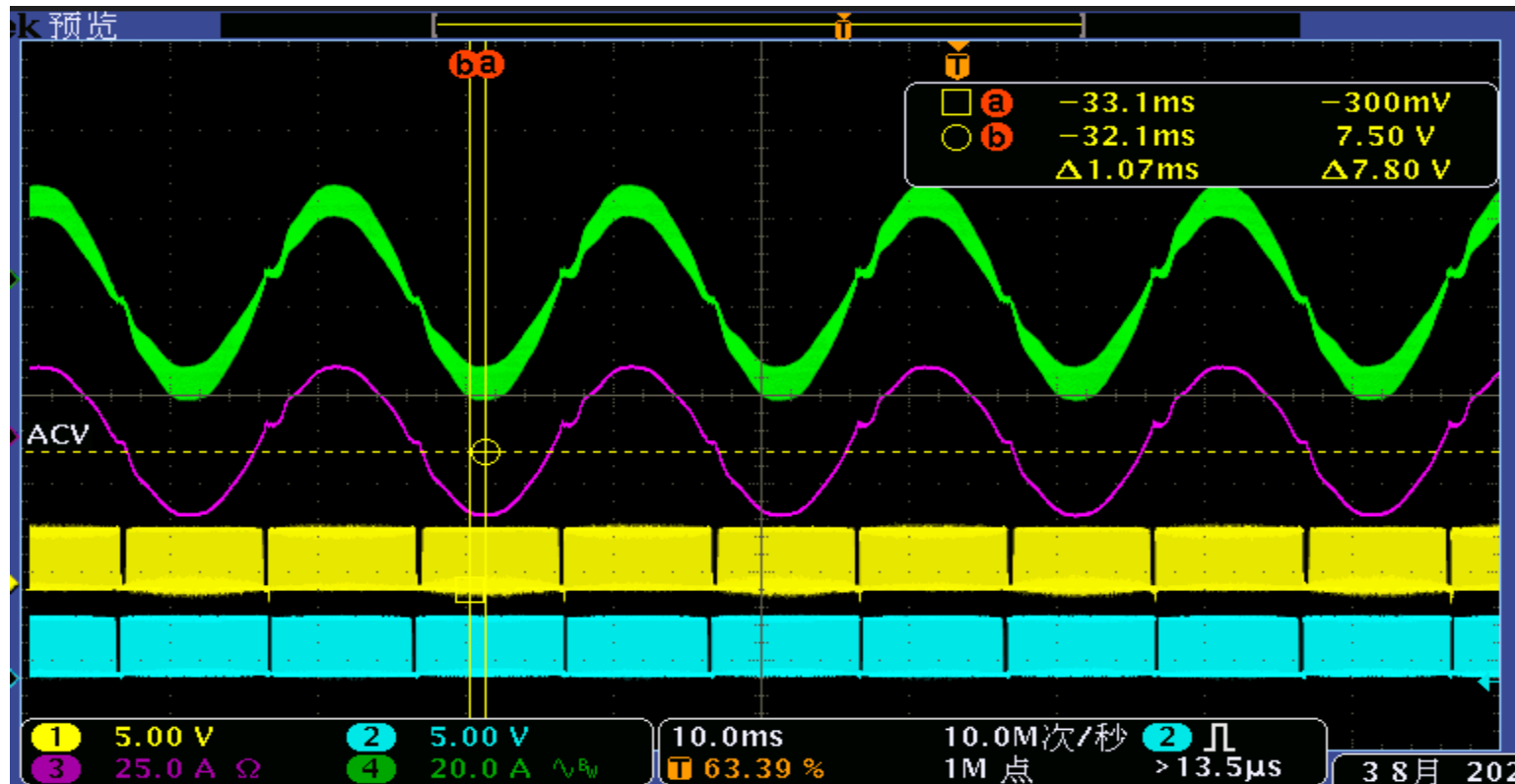
$V_{in230\&V_{out} 680V}$



$V_{in260V\&V_{out}680V}$



# EMC



AC Current (Pink), Inductor Current (Green), Switching PWM (Yellow&Blue)

Test condition  
 Vin 220Vac  
 Vout 430Vdc  
 P out 6600W

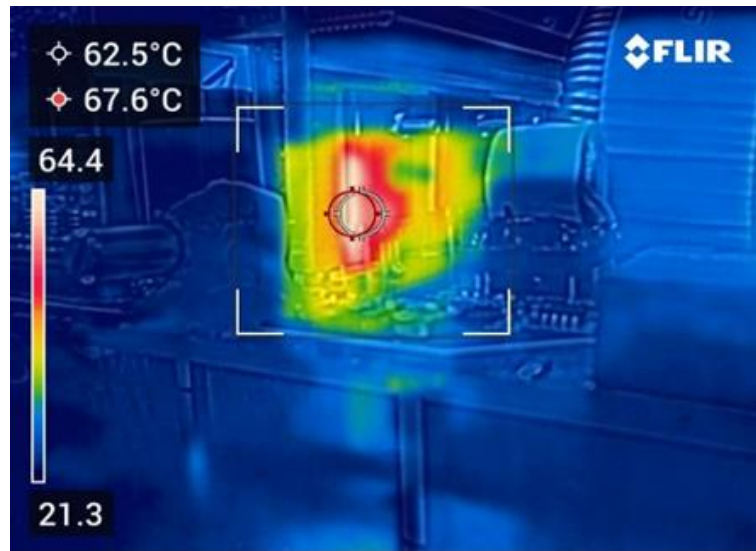
\* THDi 3.931 %  
 \* PF >0.99

# Thermal

## Test condition

Vin 220Vac  
Vout 430Vdc  
P out 6600W

Ambient Temp.: 25°C  
Delta PFB0812DHE Fan x3pcs –  
(at least 132 CFM requested)



SiC Mosfet



CLLLC Transformer



# OBC – 6.6kW Bi-directional power conversion (released)

## Key components

Function (Main Power)	Supplier	Part Number
SiC MOS	ST	SCTW40N120G2VAG
Gate Driver	ST	STGAP2SICS (1 Ch)
Resonant SMT Cap.	Murata	GCM43D7U3A472JX01L (New)
Main E-cap	Lelon	RQL221M2GBKF1846KEGA
Film cap.	Vishay	MKP1848530094K2
X-cap	Kemet	F863 series
MOV	TDK	B72220S3321K101
Fuse	Littelfuse	01220093Z/OHEV030ZXBD

Function (Aux Power)	Supplier	Part Number
LDO 3.3V	ST	LDK130M33RY
ISO DC-DC 12-12V	RECOM	REM10-1212S/A*
ISO DC-DC 12-5V	RECOM Murata	REM3-1205S/A* NCS3S4805SC*
Gate DRV ISO DC-DC 12- +/- 9V	RECOM Murata	R12P209D* NMK1209SC*

Function (DSP control)	Supplier	Part Number
MCU	ST	STM32G474RE
Crystal	Abracon	ABM3C-20.000MHz-D4Y-T
CAN Choke	Murata Bourns	DLW43SH510XK2L SRF4530A-510Y
Current Sense	Allegro	ACS770LCB-050U-PFF-T
OP-AMP	ST	TSZ181IYLY
NTC	Vishay	NTCALUG01A103F161
Ferrite Bead	Murata	BLM21PG221SH1D
Ceramic SMT Cap	Murata TDK Kemet	GRT, GRM series CGA series CXXXXXXXXXAU0
E-cap	Kemet	EDH477M025S9PAADH
Sig. Inductor	Murata	LQM2HPZ2R2MG0L
SMT Resistor	Vishay	CRCWXXXXXXXXXXJNED

**Note**

\*: Non-automotive parts



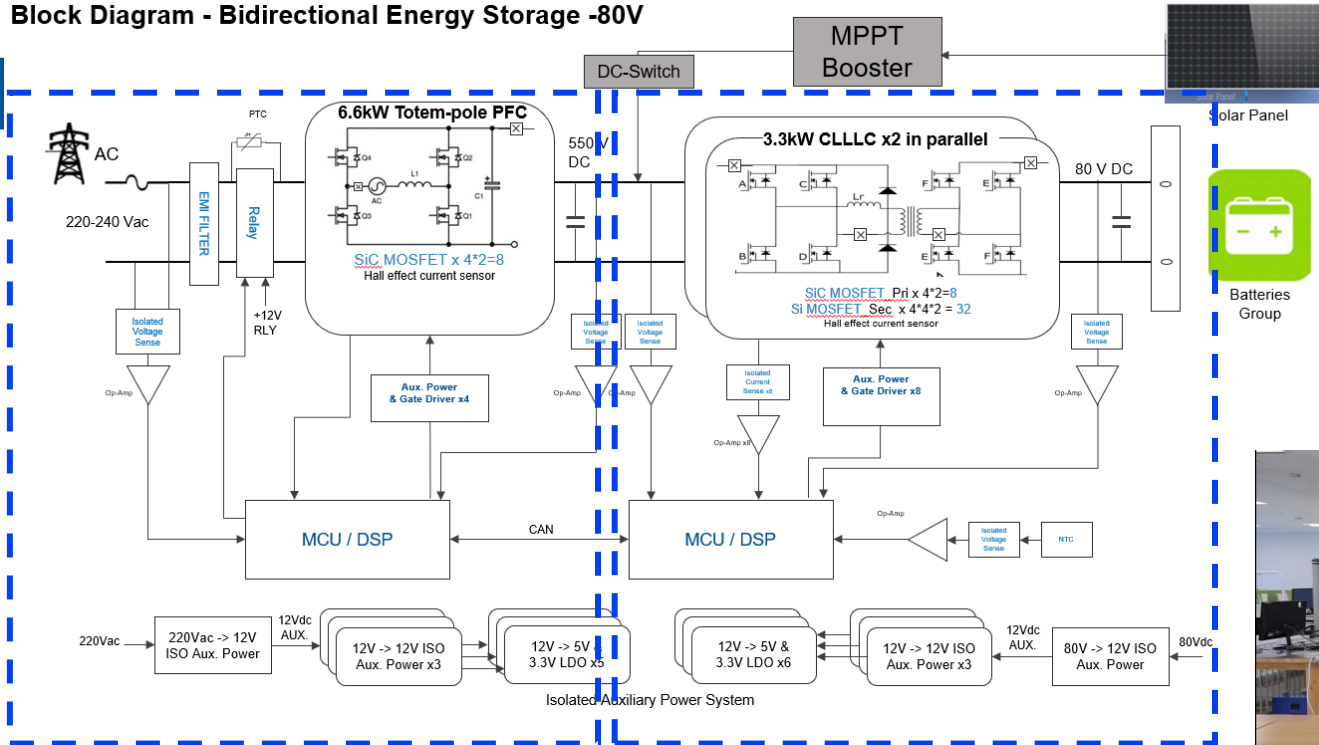
# Extension to EV charger for E-bike, Energy Storage.....



# Bidirectional Energy Storage – 80V, 82.5A/ 6600W

In Development

## Block Diagram - Bidirectional Energy Storage -80V



PFC: Lx Wx H= 450mm x 150mm x 100 mm

**Bidirectional PFC**  
**(Released)**

**Demo video**

[https://www.arrowopenlab.com/hk/solution\\_video\\_article/2021P005\\_en.html](https://www.arrowopenlab.com/hk/solution_video_article/2021P005_en.html)



DC-DC Lx Wx H= 450mm x 330mm x 100 mm

**Bidirectional DC-DC**  
**(Release by Q4'22)**



Batteries Group



### Specification:

- AC/DC Bidirectional Power Conversion
- Max Charging Power: 6.6kW
- AC Input Voltage: 180-265 VAC
- DC Output Power: 60-90VDC
- Max Inversion Power: 6.6kW
- Inversion Rated Input: 80Vdc
- Inversion rated Output: 220Vac 50Hz
- Efficiency >95%
- Totem Pole PFC 120 kHz
- CLLLC 200kHz
- Forced Cooling

### Applications:

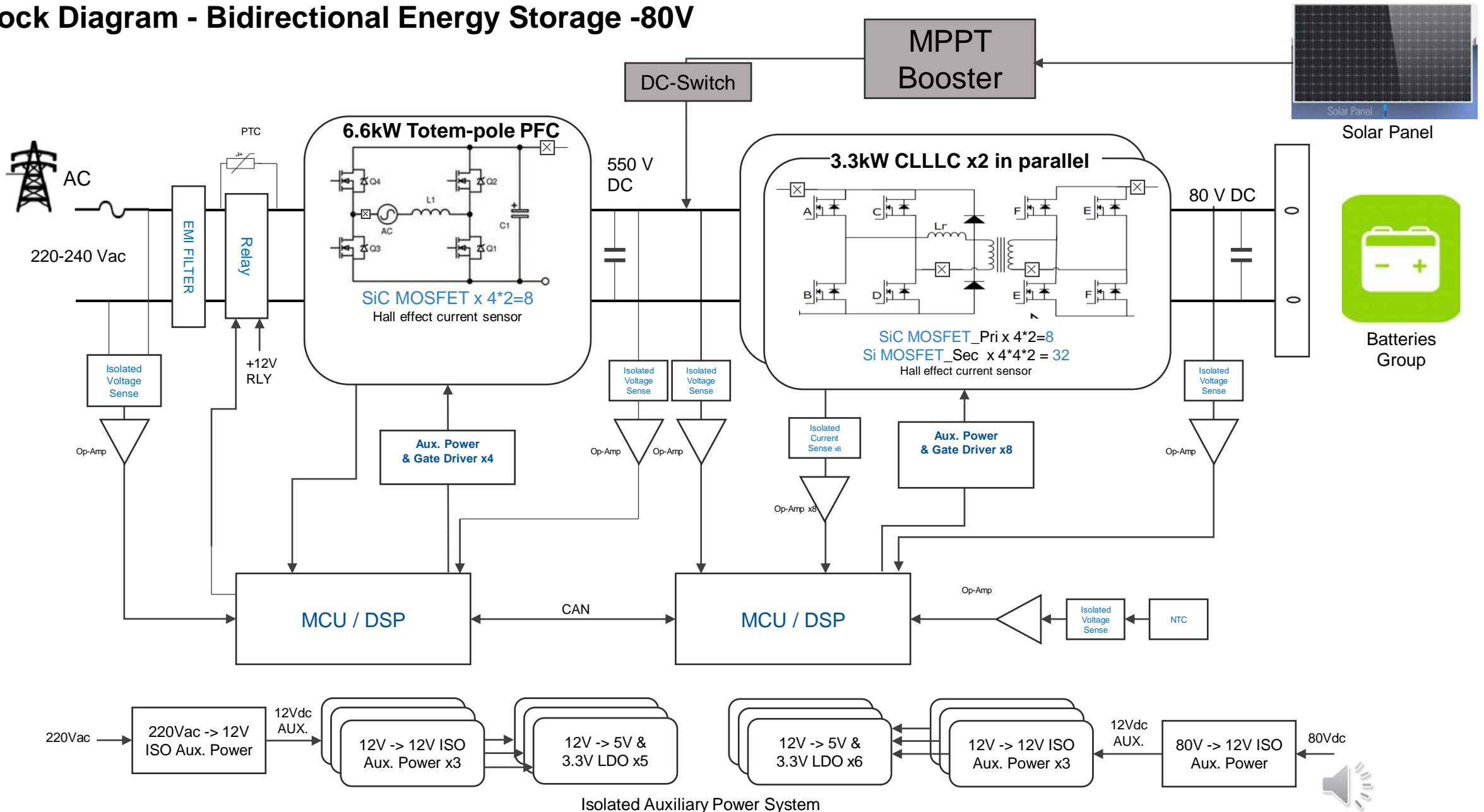
- Energy Storage
- Solar inverter with energy storage
- Forklift Charger
- AC-DC loading equipment

### Key ST Parts

Functions	Qty	Devices
SiC MOS	16	SCTWA60N120G2-4
SiC MOS Gate Driver- 1-CH	8	STGAP2SiCS
Gate Driver Isolated Power	12	L6986I
DC-DC low side FET	32	STP75NF20
Diode	2	STPS1150A
Isolated DC-DC/10W	6	STL8N10LF3*
MCU	2	STM32G474VBT6

Functions	Qty	Devices
Aux	1	VIPER319HDTR
ESD Suppression	3	HDMIULC6-4SC6Y
ESD Suppression	2	ESDCAN03-2BWY
Hi-Precision OP-AMP	1	TSZ181ILT
Processor Supervisor	1	STM6825TWY6F
Digital Isolator	2	STISO621WTR

# Block Diagram - Bidirectional Energy Storage -80V



# 15kW Bidirectional PFC

## Front-end Power Converters



### ★ specifications

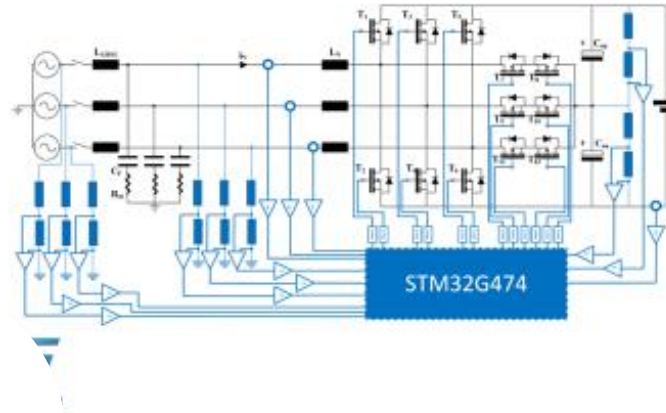
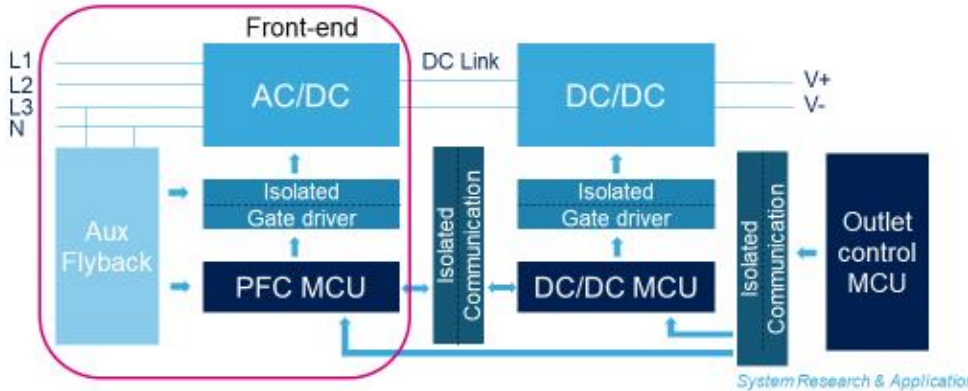
$V_{AC}$	400 Vac
$V_{DC}$	800 Vdc
$P_{Out\_max}$	15 kW
$F_s$	70 kHz
$I_{ripple}$	2.5A
$V_{out\_ripple}$	10 Vpp
PF	> 0.9
THD	< 5%

## STDES-PFCBIDIR Demoboard



Control board

System Research & Applications – Power Conversion



# Digital Power Control - MCU

# MCU STM32G474

## > Accelerator-- CORDIC

### • STM32G4 CORDIC 支持以下的函数:

- 余弦Cosine ( $\cos \theta$ )
- 正弦Sine ( $\sin \theta$ )
- 相位Phase ( $\text{atan2 } y,x$ )
- 取模Modulus ( $\sqrt{x^2 + y^2}$ )
- 反正切Arctangent ( $\tan^{-1} x$ )
- 双曲正弦Hyperbolic sin ( $\sinh x$ )
- 双曲余弦Hyperbolic cosine ( $\cosh x$ )
- 双曲反正切Hyperbolic arctangent ( $\tanh^{-1} x$ )
- 自然对数Natural logarithm ( $\ln x$ )
- 平方根Square root ( $\sqrt{x}$ )

q1.15 fixed point:  
(precision = 4)

ARM fast math arm_sin_q15()	Cordic: zero-overhead mode	Cordic: DMA in/out mode
36 cycles/sample	7 cycles/sample	11 cycles/sample
-	x5 acceleration	x3 acceleration
100%CPU	100% CPU	0% CPU
Max error: 0.00012	Max error: 0.00004	Max error: 0.00004
-	x3 precision	x3 precision

q1.31 fixed point:  
(precision = 6)

ARM fast math arm_sin_q31()	Cordic: zero-overhead mode	Cordic: DMA in/out mode
41 cycles/sample	8 cycles/sample	12 cycles/sample
-	x5 acceleration	x3 acceleration
100%CPU	100% CPU	0% CPU
Max error: 0.00002	Max error: 0.000002	Max error: 0.000002
-	x10 precision	x10 precision

# MCU STM32G474

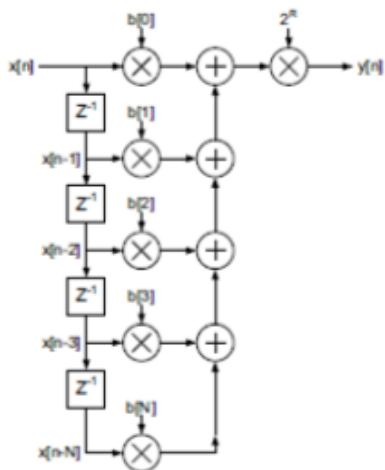
> Accelerator-- FMAC

## 数字滤波加速器(FMAC)

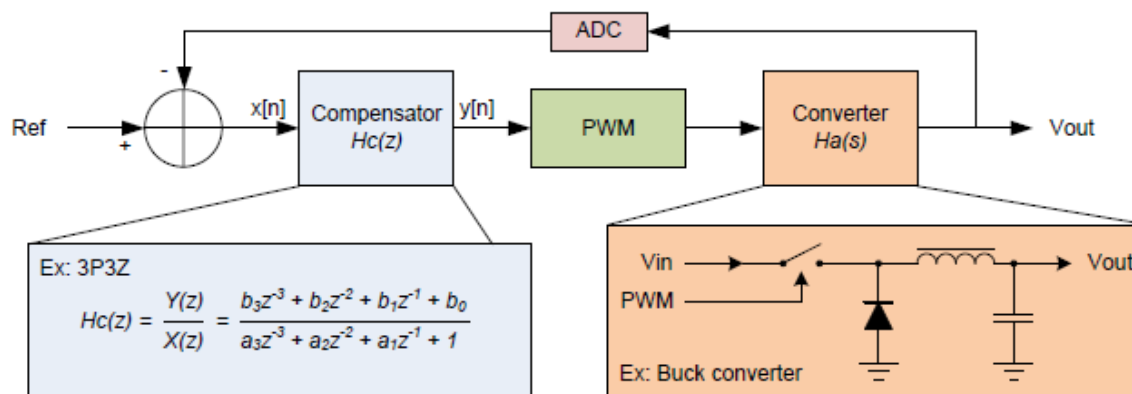
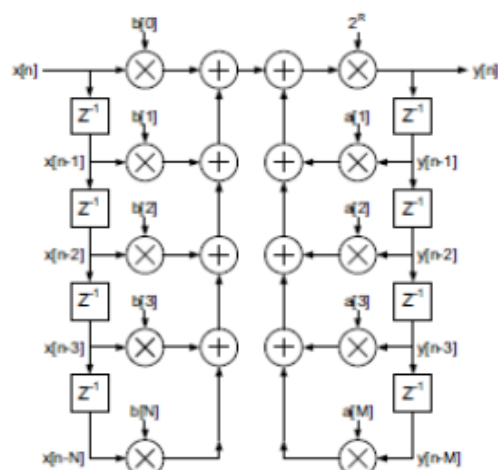
• 可被用于生成

- FIR, IIR
- 补偿器 (数字电源三极点三零点3p3z)

### FIR 滤波器



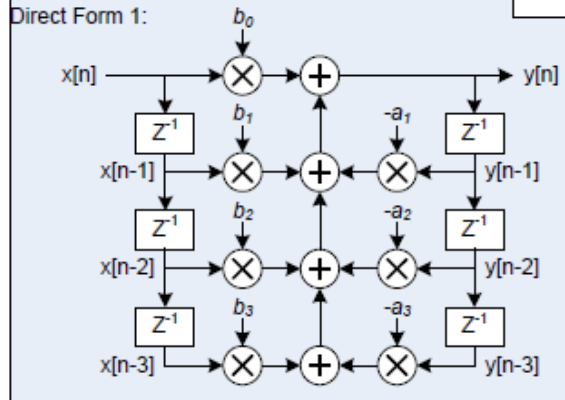
### IIR滤波器



Ex: 3P3Z

$$H_c(z) = \frac{Y(z)}{X(z)} = \frac{b_3z^{-3} + b_2z^{-2} + b_1z^{-1} + b_0}{a_3z^{-3} + a_2z^{-2} + a_1z^{-1} + 1}$$

$$y[n] = b_0x[n] + b_1x[n-1] + b_2x[n-2] + b_3x[n-3] - a_1y[n-1] - a_2y[n-2] - a_3y[n-3]$$



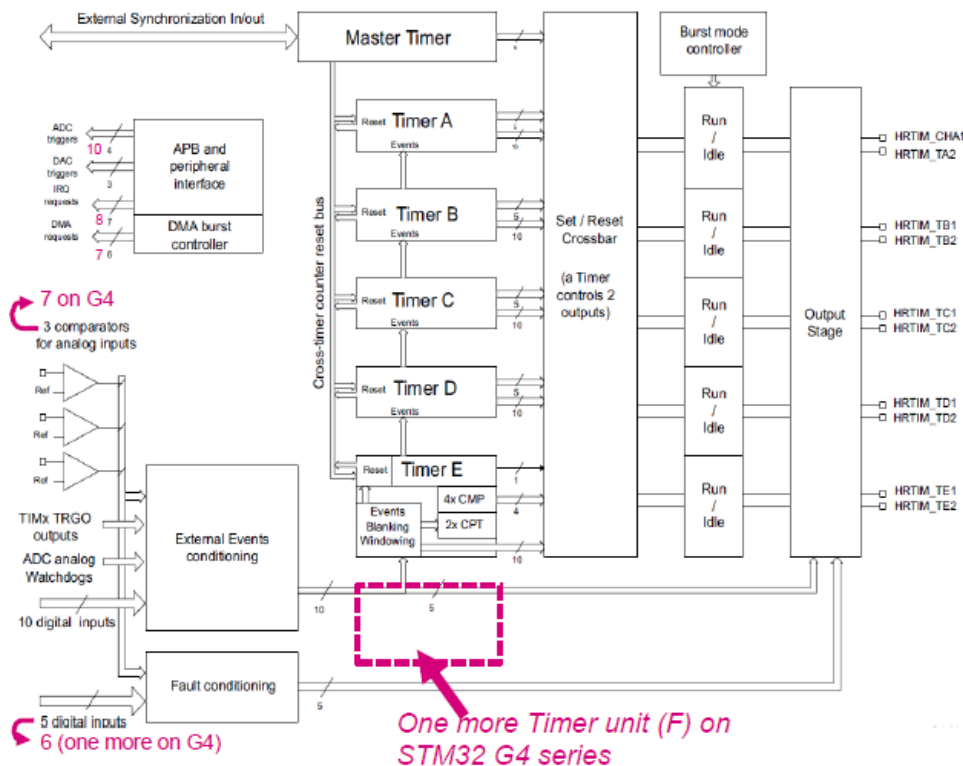
FMAC configuration:  
 X1\_BUF\_SIZE ≥ 5, X2\_BUF\_SIZE = 7, Y\_BUF\_SIZE ≥ 4  
 Preload X2\_BUF : [b0,b1,b2,b3,a1,a2,a3]  
 Run IIR filter with parameters: P = 4, Q = 3  
 Repeat:  
 Write x[n] to WDATA  
 Poll YEMPTY flag low or wait for interrupt (~8 clock cycles)  
 Read y[n] from RDATA



# MCU STM32G474

## > HRPWM

- 模块架构: 主定时器+ 6 x 子定时器, 交叉同步
- 主频: 170MHz, DLL 32x to 5.4G
- 高精度
  - 184ps 所有PWM输出
- 自动校准
  - 无温漂/电压偏移
- 高达12路PWM输出
- 多种故障/事件输入
- 减少软件开销
- 复合事件处理机制
  - 消隐/窗口/超时



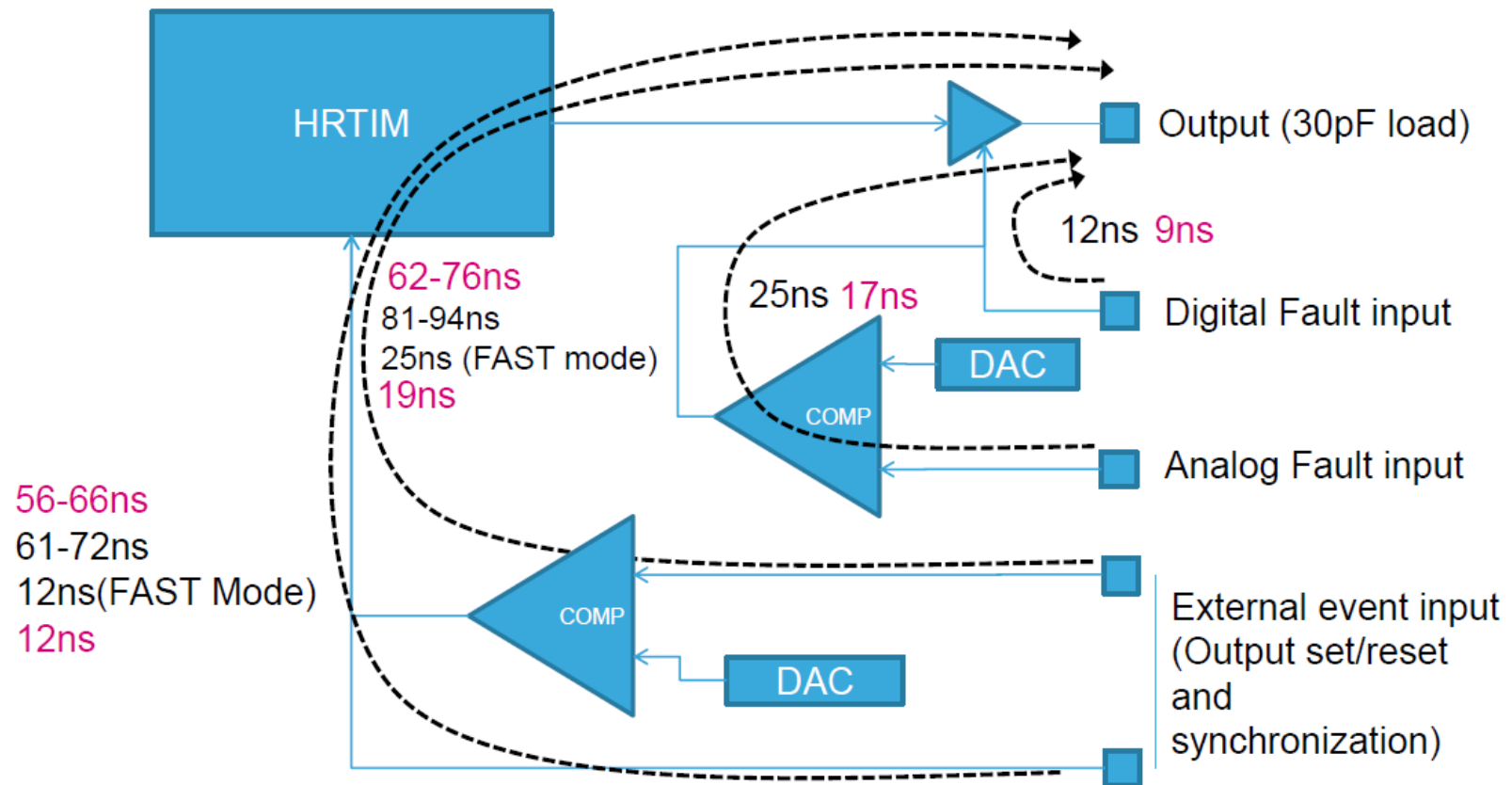
# MCU STM32G474

## > ADC

ADC 单元	5 (only 2 for G431)
输入通道	高达42路输入, 单端/差分模式 (only 18 for G431)
转换技术	12-bit 逐次逼近
转换时间	250 nS, 4 Msamples/s (when $f_{\text{ADC\_CLK}} = 60 \text{ MHz}$ )
转换模式	单次(singal)、连续(continuous)、扫描(scan)、不连续(discontinuous)、注入(injected)
触发启动	软件启动或是外部事件触发启动(定时器或是IO)
特殊功能	硬件过采样, 模拟看门狗 (+滤波), 数据预处理 (偏置和增益补偿), 多种采样时间设定
数据处理	中断, DMA 请求
低功耗模式	Deep power-down, auto delay, 功耗取决于转换速度

# MCU STM32G474

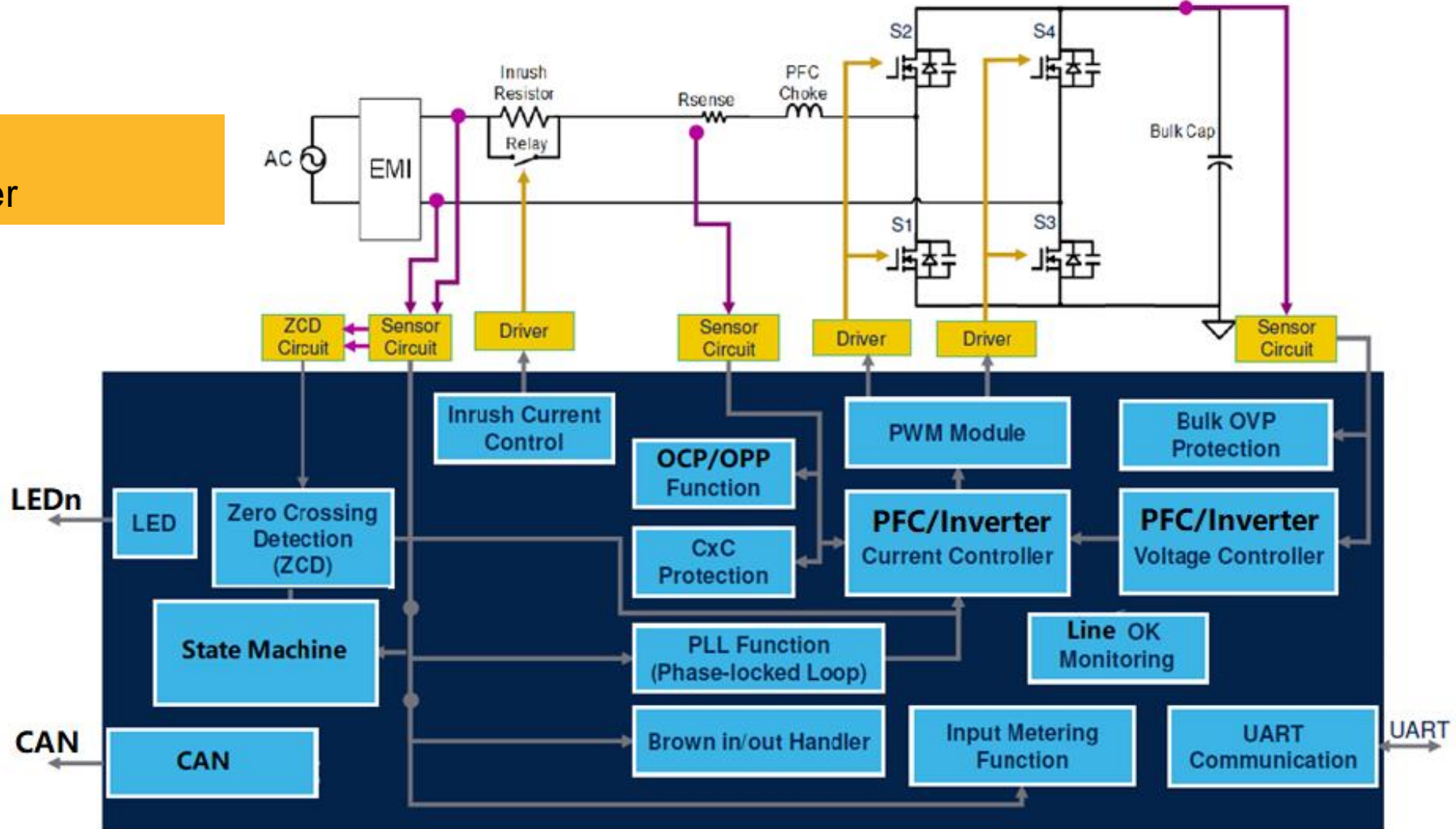
> Fast protection response



# Digital Power Control - Firmware

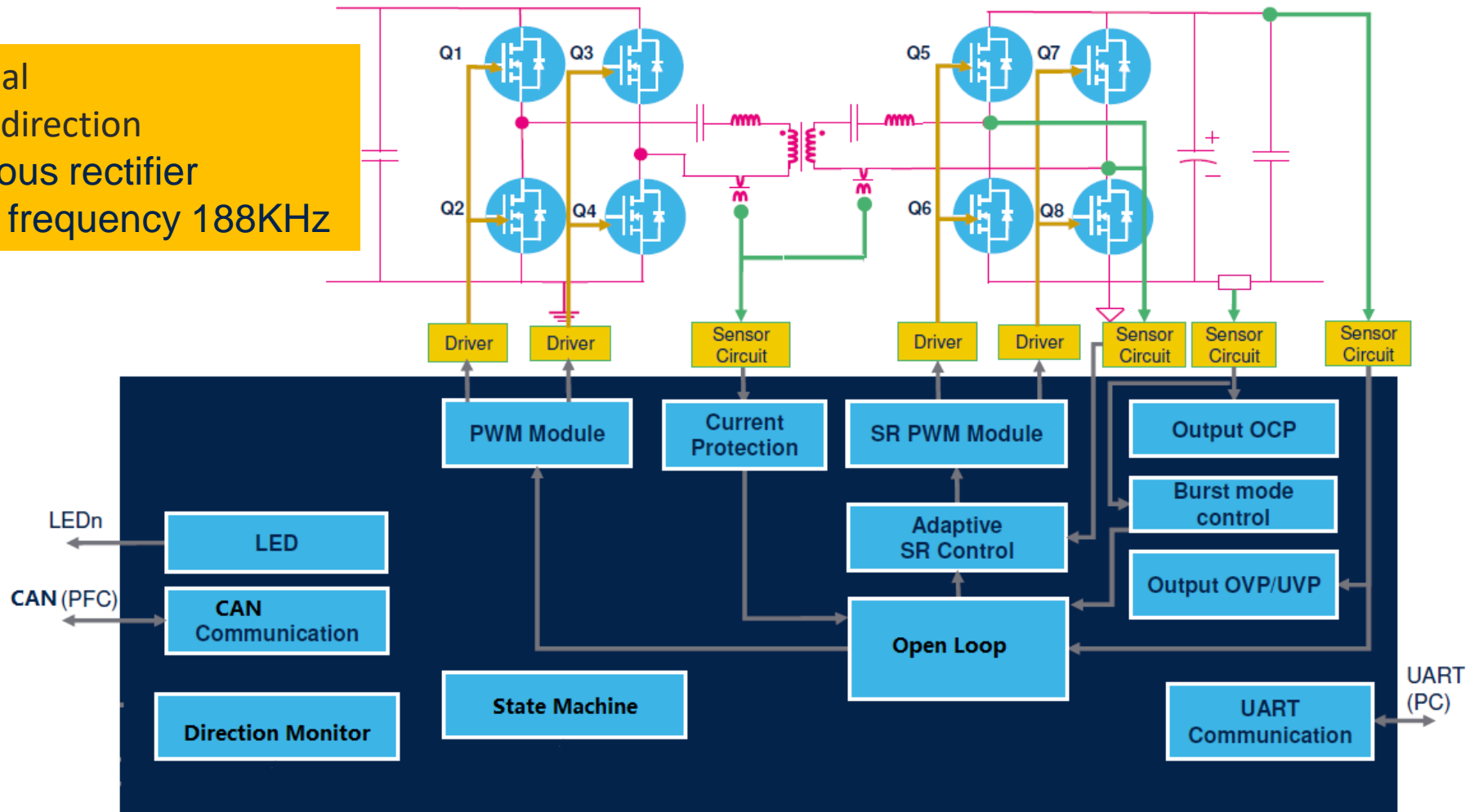
# PFC/Inverter Functional Block Diagram

- PFC
- Inverter

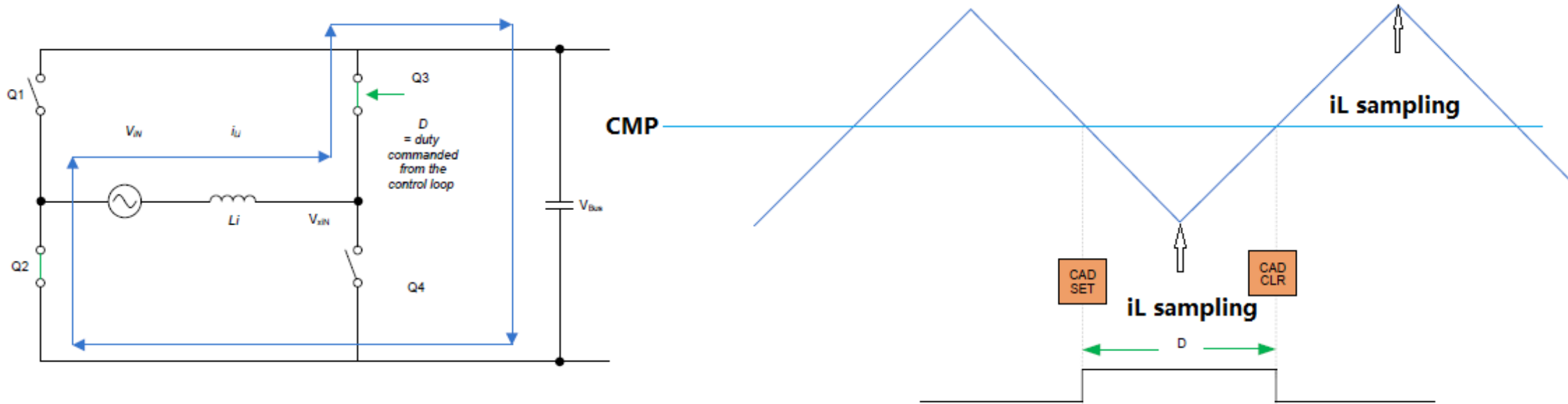


# CLLLC Functional Block Diagram

- Bidirectional
- Adaptivity direction
- Synchronous rectifier
- Resonant frequency 188KHz



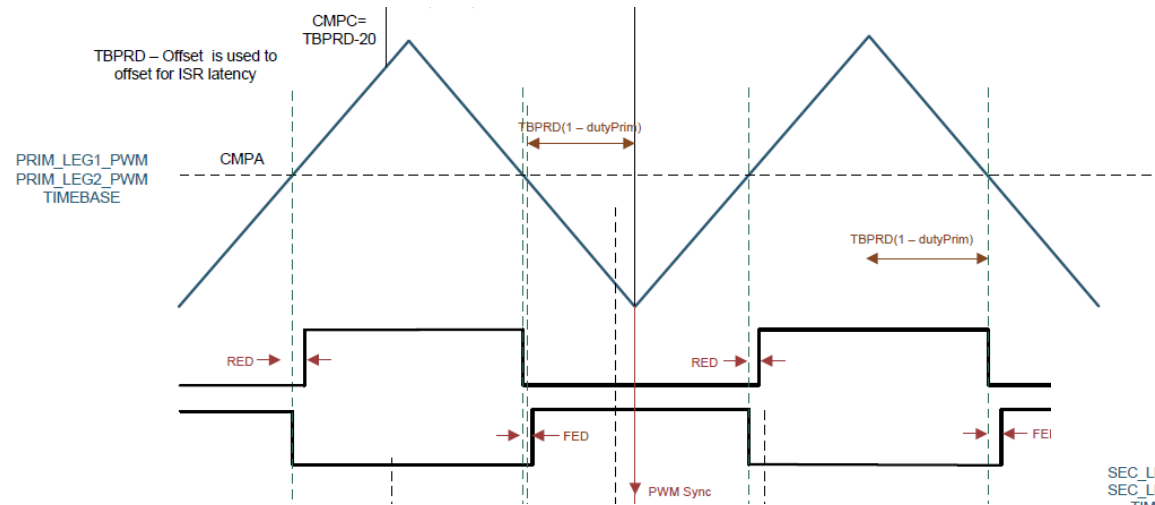
# PWM Generate & Current sampling For PFC



Single-Phase Diagram of TTPL PFC

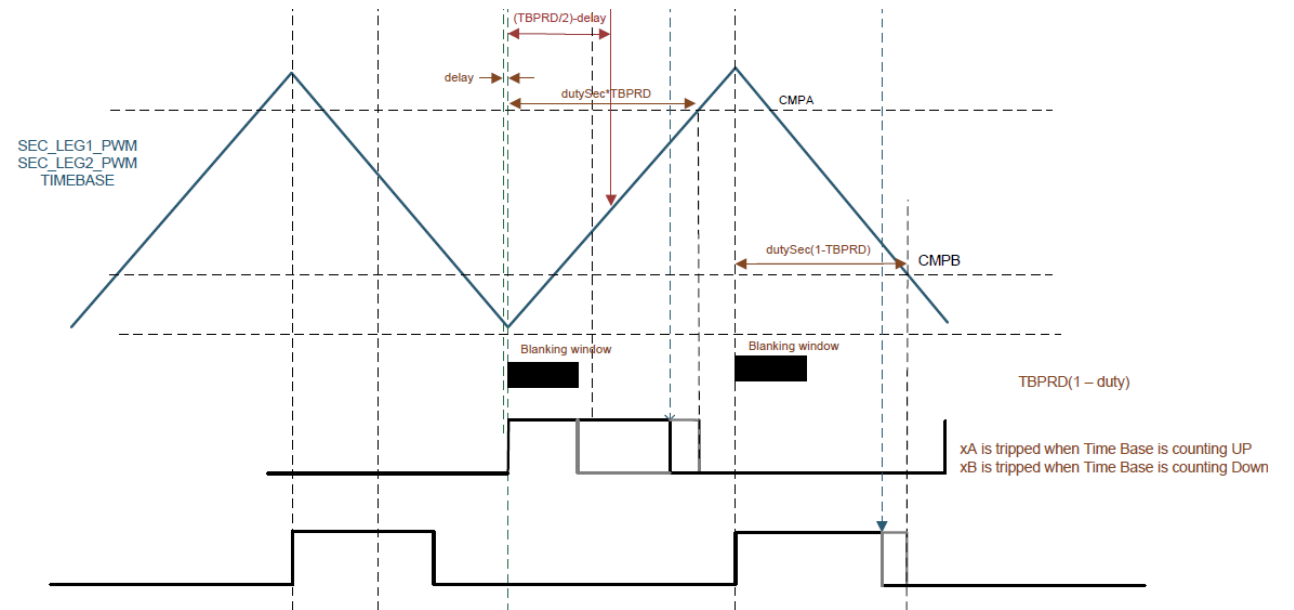
Inductor current is sampled twice per PWM switching cycle · averaged twice before being used as the current loop feedback input. It can mainly reduce the interference during sampling and ensure the balance of positive and negative half cycles.

# PWM Generate For CLLLC



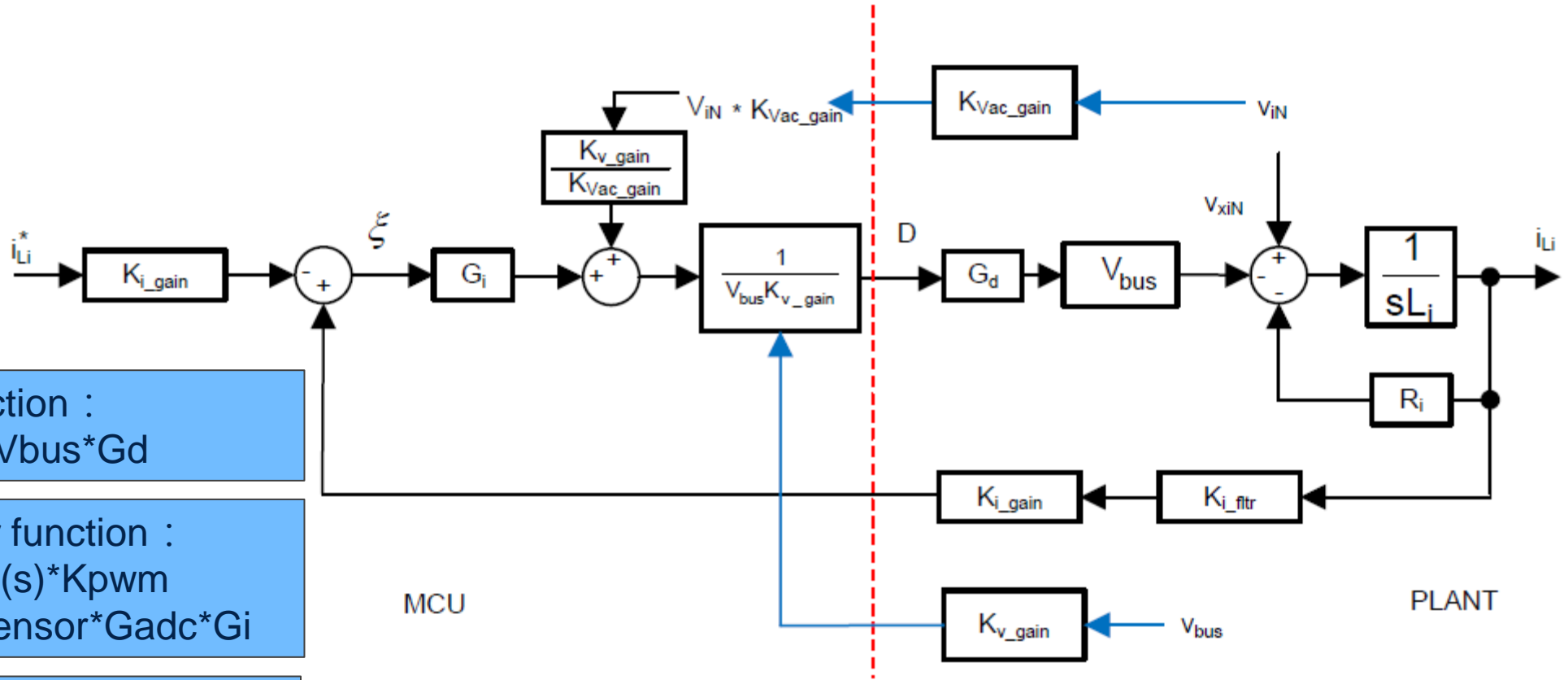
Primary Side PWM

## Second Side PWM





# Current Loop Block Diagram For PFC

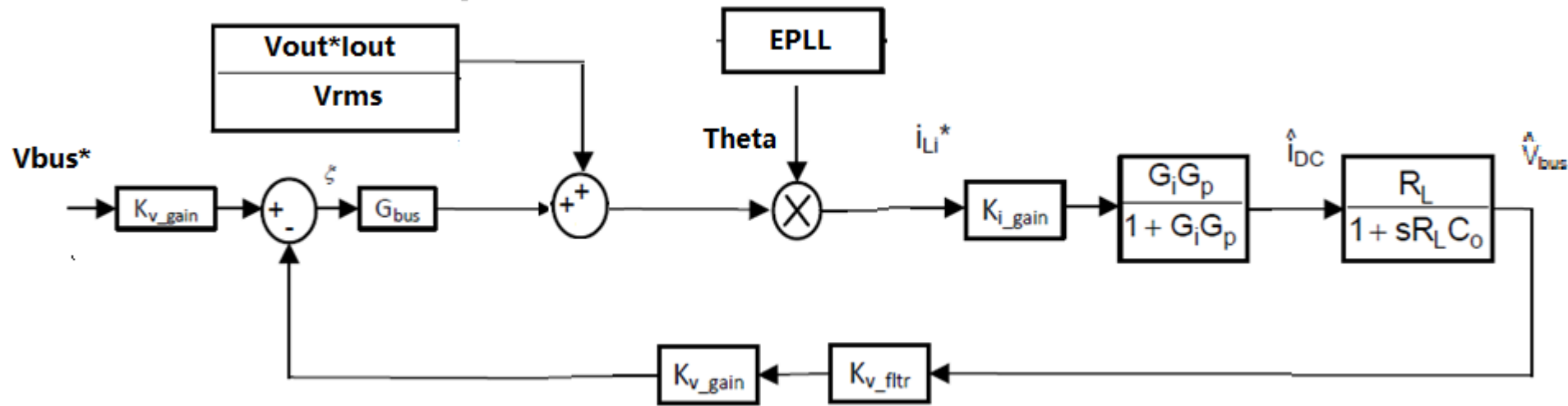


Plant transfer function :  
 $Plant(s) = (1/sL_i) * V_{bus} * G_d$

Open loop transfer function :  
 $I_{Plant}(s) = Plant(s) * K_{pwm} * G_{i\_sensor} * G_{adc} * G_i$

Control algorithm: PI

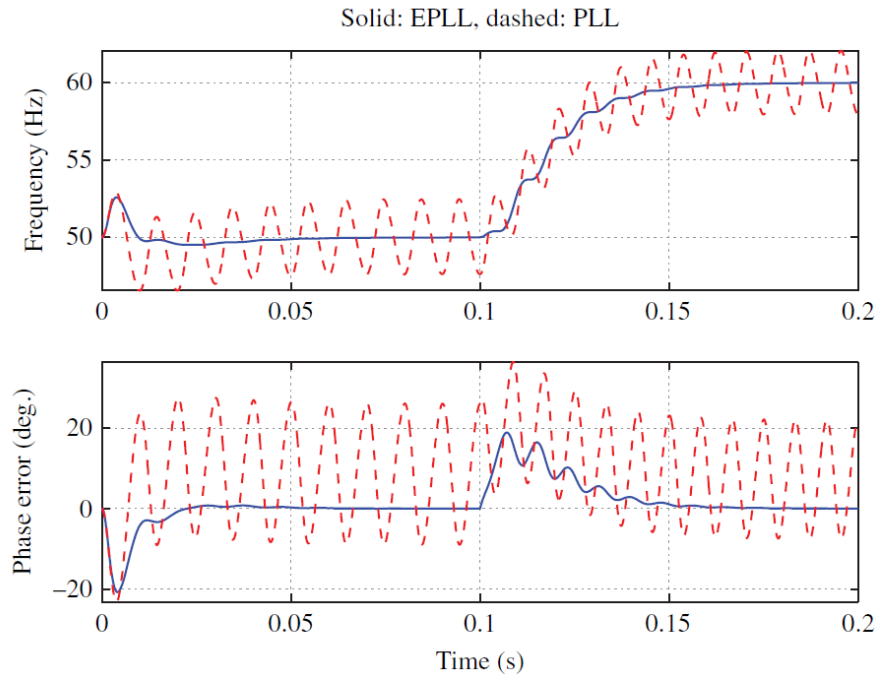
# Voltage Loop Block Diagram for PFC



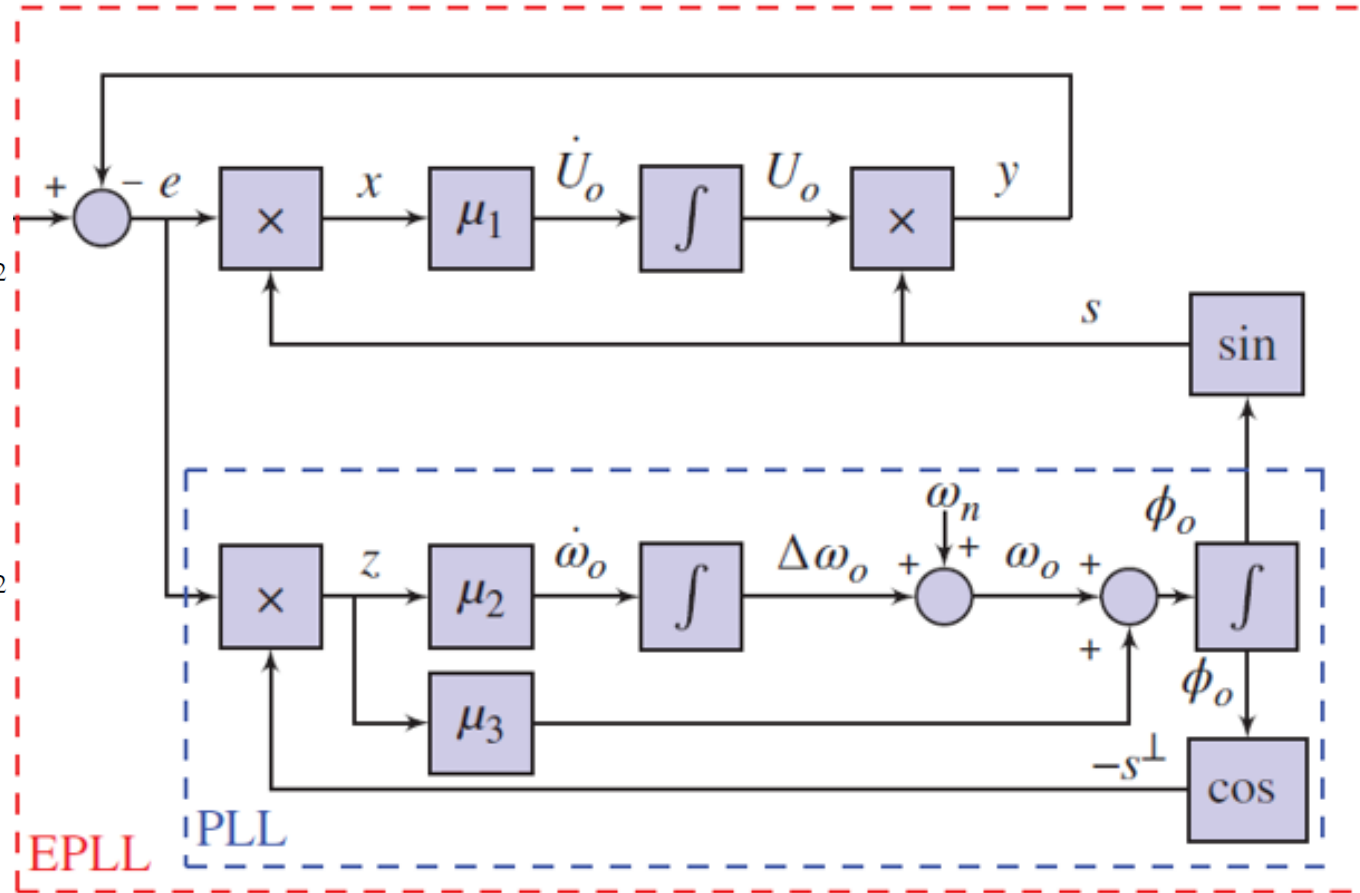
Control algorithm: PI

- Voltage loop: performed at 10kHz
- Current loop: performed at 67kHz

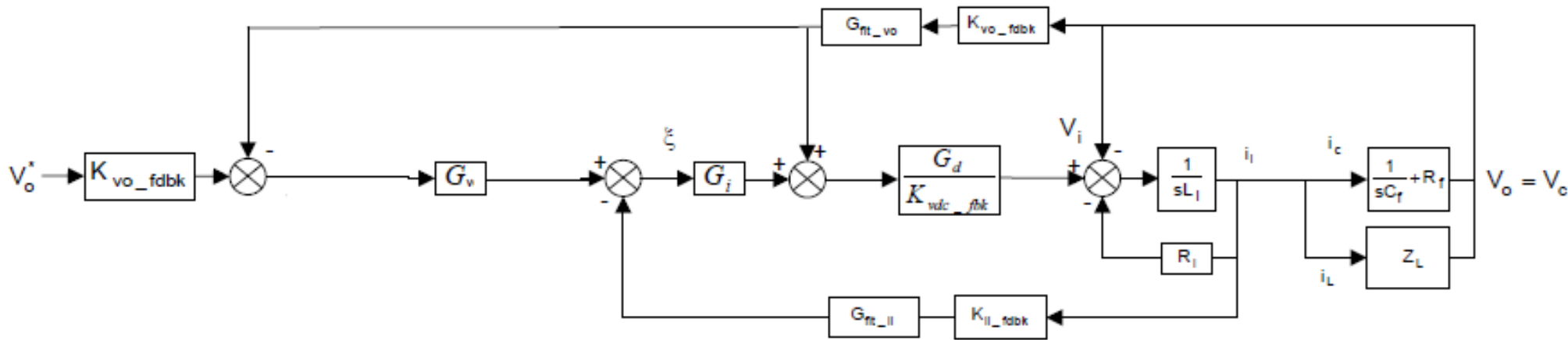
# EPLL Block Diagram for PFC



$$\begin{aligned}
 x &= e \sin\phi_o = (U_i \sin\phi_i - U_o \sin\phi_o) \sin\phi_o \\
 &= \frac{U_i}{2} \cos(\phi_i - \phi_o) - \frac{U_o}{2} + \underbrace{\frac{U_o}{2} \cos(2\phi_o)}_{\text{double frequency}} - \frac{U_i}{2} \cos(\phi_i + \phi_o)
 \end{aligned}$$



# Voltage & Current Loop Block Diagram for Inverter

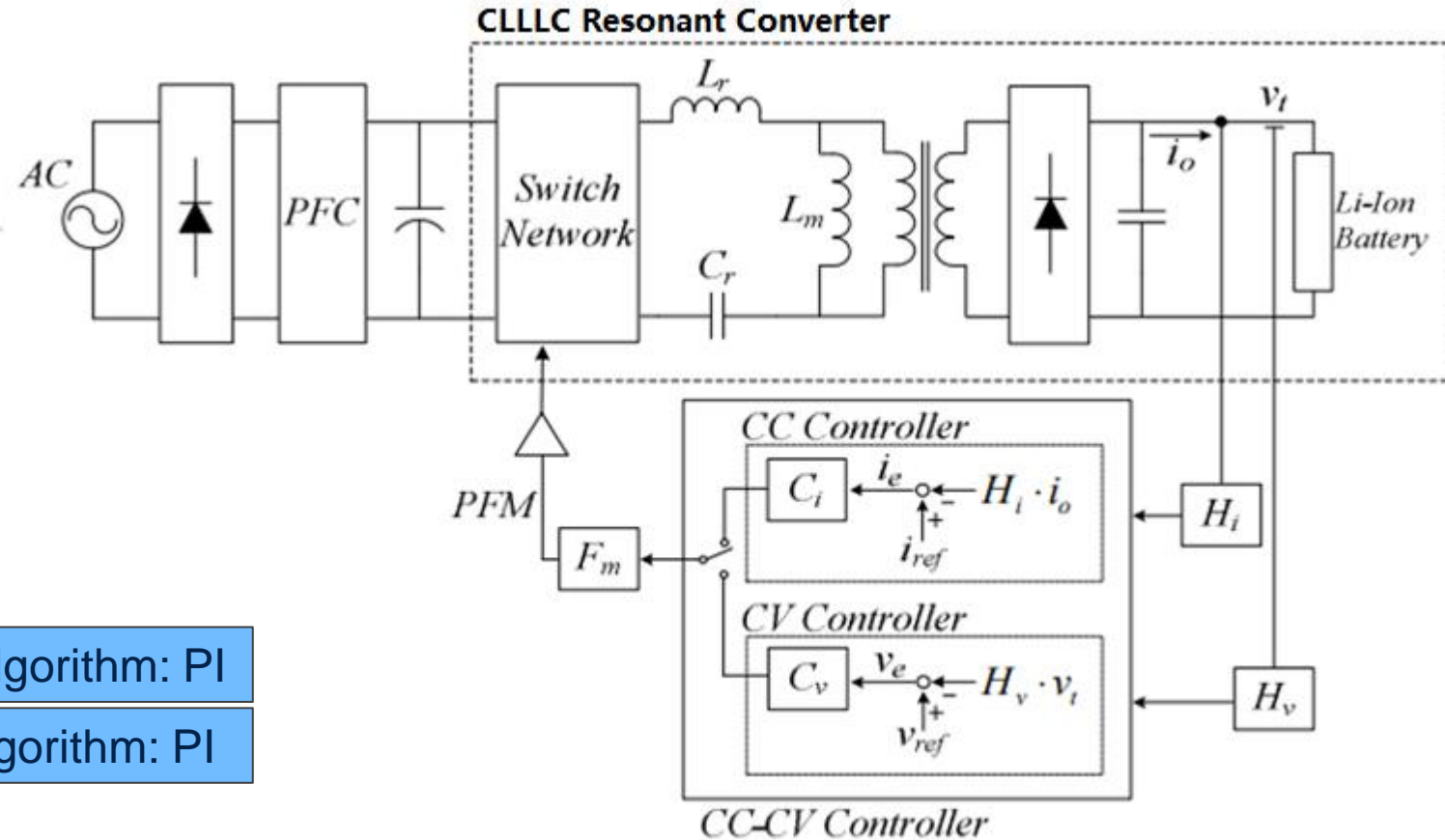


Current Loop Control algorithm: PI

Voltage Loop Control algorithm: PI

- Voltage loop: performed at 67kHz
- Current loop: performed at 67kHz

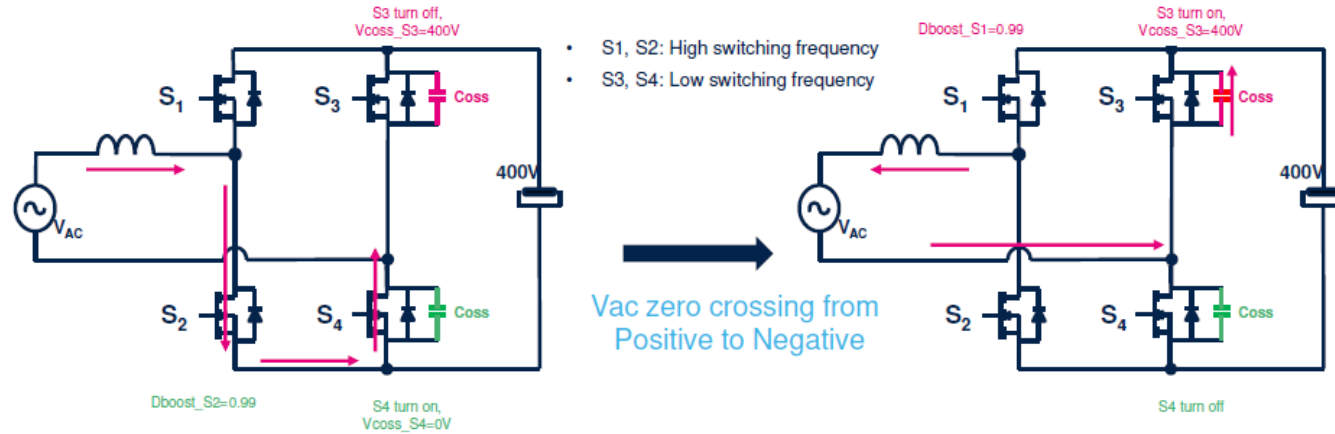
# CC&CV Controller for CLLC



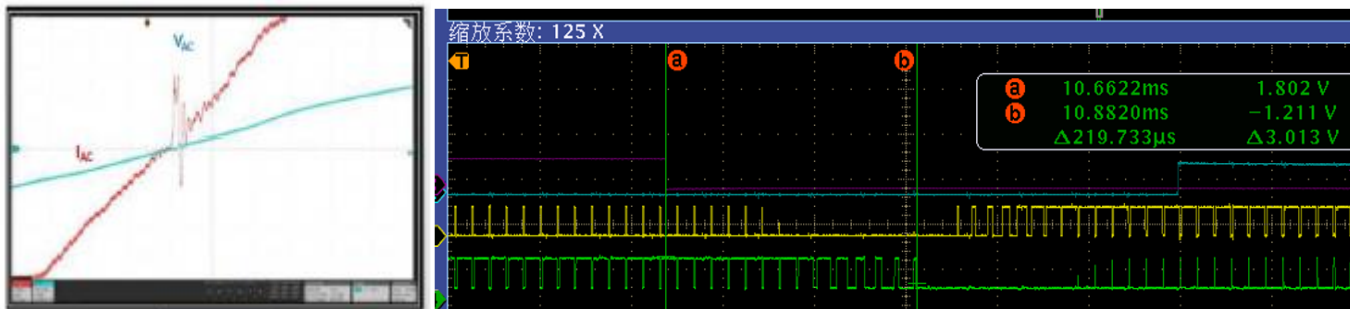
Current Loop Control algorithm: PI

Voltage Loop Control algorithm: PI

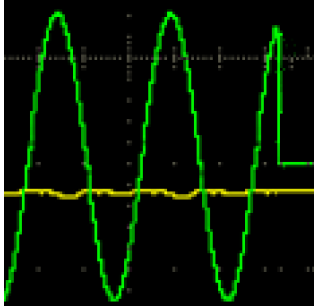
# Design challenge 2 : Current spike at AC zero crossing



- The control loop should freeze during the blanking time, in order to avoid the integrator of the current loop to generate a large PWM pulse, which will cause a large current spike
- PWM soft-start at zero crossing
- All MOSFETs are turned OFF to ensure a safe permutation of the power switches control and to avoid short-circuit of the output DC capacitor



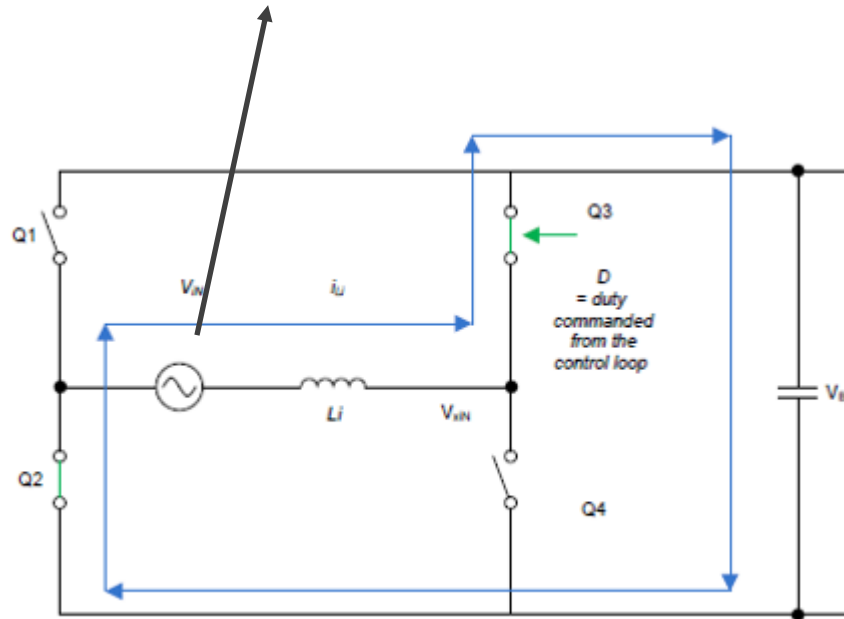
# Design challenge 3 : Vac Drop (Under-voltage) Control



In PFC Charging mode, if the voltage of line drop to zero from higher voltage positions, what will happen?



If the mains drops from high voltage to Zero in PFC mode, the working state is changed from PFC to Inverter mode. At this moment, it is equivalent to the short circuit of the inverter output.

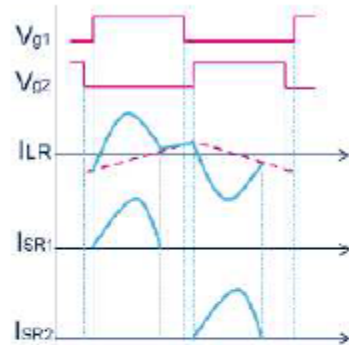


Solution:

- Add Grid Voltage drop Monitoring in Software
- Add Over-current Protection Detection at AC input side

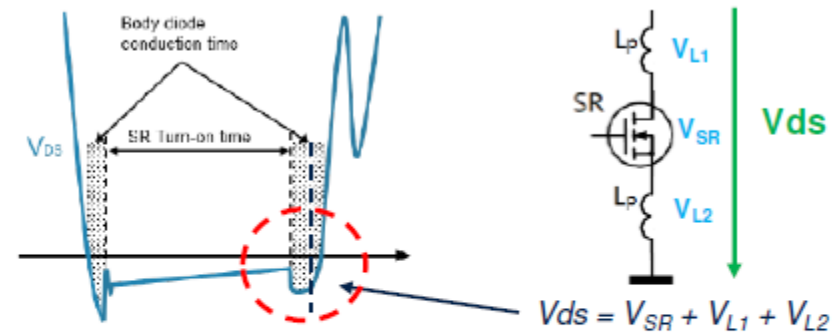
# Design challenge 4 : Synchronous rectifier(SR) control

- Negative current caused by late SR MOSFET turn-off



- At heavy load (below resonant frequency), late SR turn off will force MOSFET conduct and cause a negative current from output capacitor
- This negative current could damage the power MOSFETs and resulting unit failure

- Premature SR MOSFET turn-off



- Due to the stray inductance in series with the SR MOSFET, the sensed drain-source signal ( $V_{ds}$ ) is not really the voltage drop across the SR MOSFET ( $V_{SR}$ )
- So it will prematurely turn-off SR MOSFET and cause low efficiency



# Arrow Technical Support Contacts

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**Thank You !**  
**Q & A**